



ETICS with vacuum insulation panels for retrofitting buildings from the great Swedish housing program “Miljonprogrammet”

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Robust and Durable Vacuum Insulation Technology for Buildings

KTH

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Why the Swedish "Million program"?

We have to deal with the existing building stock - to meet the "20-20-20" targets of the EU-commission related to climate and energy

In Sweden, about 21% of the energy use can be related to the heat losses through the climatic envelopes of buildings

The Swedish "Million Program" units built in the period between 1965 and 1974

A U-value of about 0,6 Wm⁻²K⁻¹ on average for external walls



Rinkeby, Stockholm



Fittja, Stockholm



Skärholmen, Stockholm



Tensta, Stockholm



Objectives

- To propose a new and robust VIP technical solution for the great Swedish Million dwelling program
- To investigate the influence of various design factors on the resulting U-value
- To simulate heat and moisture conditions.
- To compare theoretical assessments and in situ measurements of thermal performance
- To carry out a full scale measurement in a climatic chamber to investigate the influence of thermal bridges of a wall construction with exterior VIPs

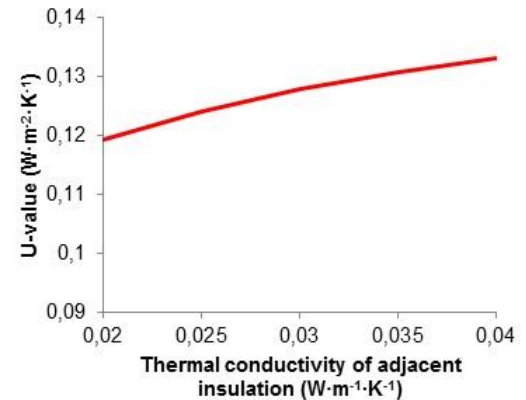
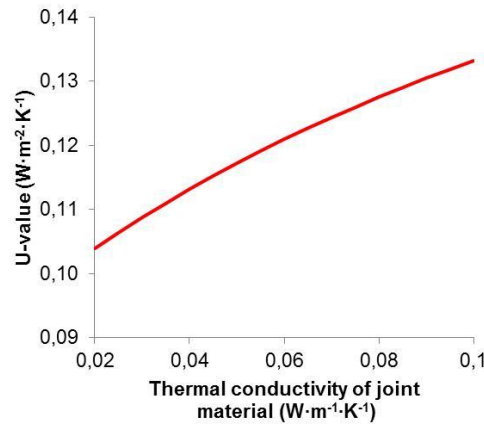
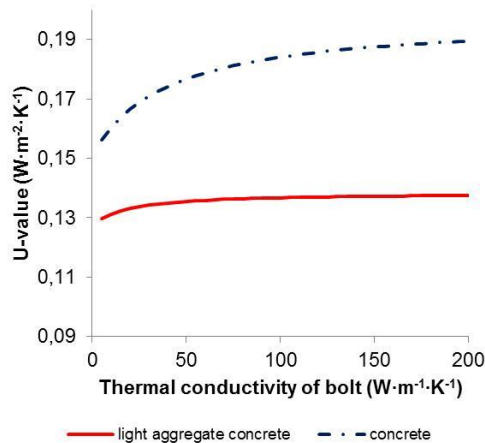
Method

- *A parametric study of the impact of the thermal conductivity of the joints of the panels and the adjacent insulation layer as well as the material of the fasteners*
- *A 3-dimension COMSOL simulation of heat transfer through the construction*
- *A 2 dimensional transient modeling of vapor diffusion with COMSOL allowing for sorption in the material as well as enhanced moisture transport at high relative humidity.*



Hovsjö, an example of a housing project in the “Million Program”

Parametric pre-study

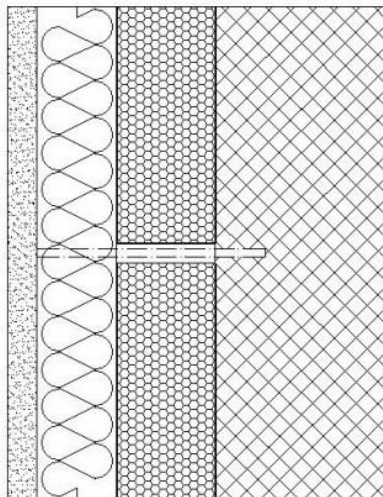


- The material with a high thermal resistance at the VIP joints has a significant influence on the thermal bridges. Going from a value of 0.10 to 0.02 $\text{W m}^{-1}\text{K}^{-1}$ will give a reduction that amounts to about 30% of the total density of heat loss
- The influence of improving the outer insulation layer does also have a measurable effect on the heat flux, although somewhat smaller.

VIP technical solution

2D och 3D dynamic simulations with Comsol Multiphysics®

- *The average hourly values for outdoor temperature and relative humidity are retrieved from an International weather for energy calculation (IWECC) climate file for Stockholm, 2012*
- *The indoor temperature and relative humidity are as defined by EN 15026*

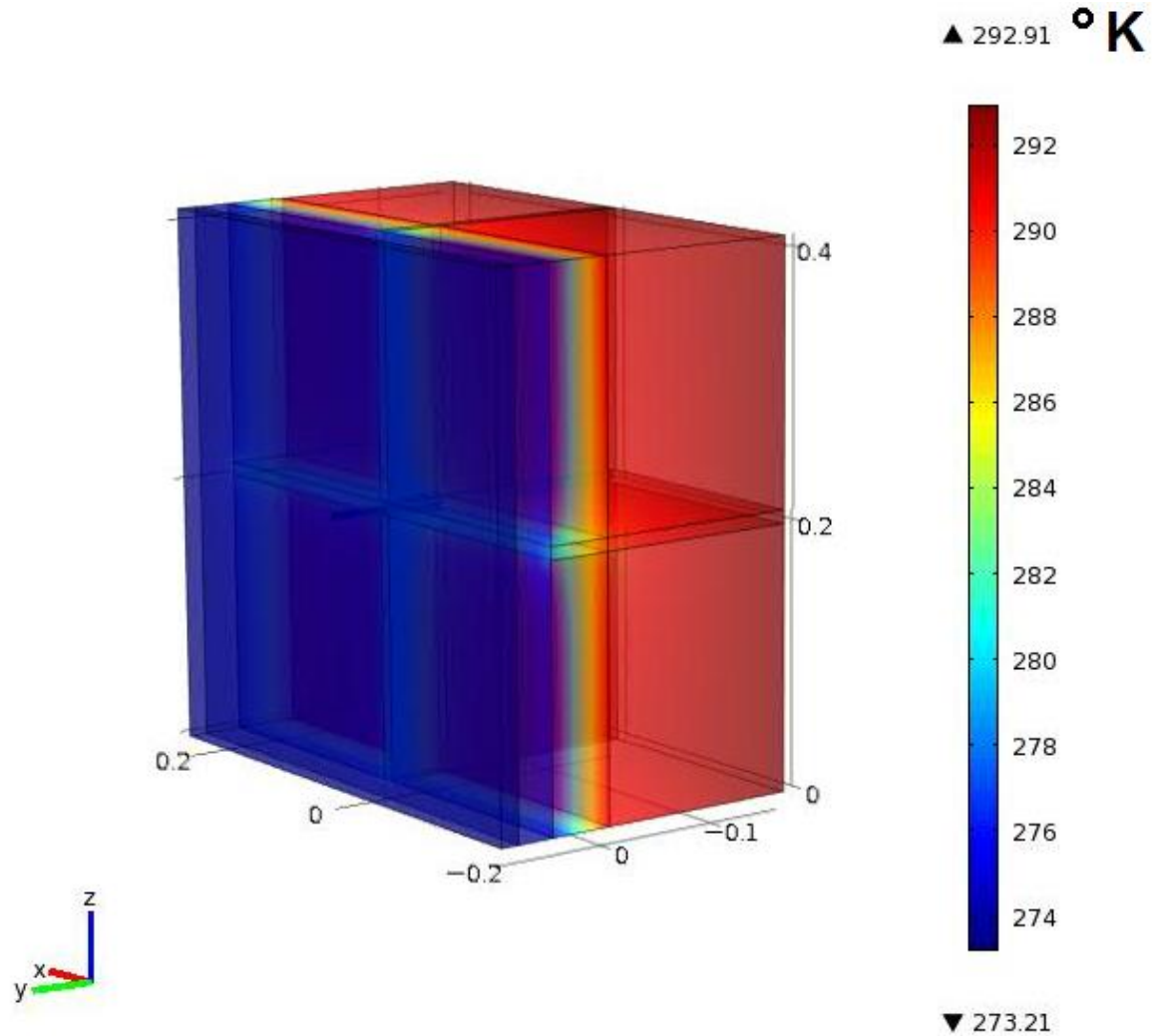


≠ Ø_{bolt}

15 RENDERING
45 MINERAL WOOL
50 VIP , WITH A 10 MM JOINT BETWEEN
PANELS
160 LIGHT AGGREGATE CONCRETE

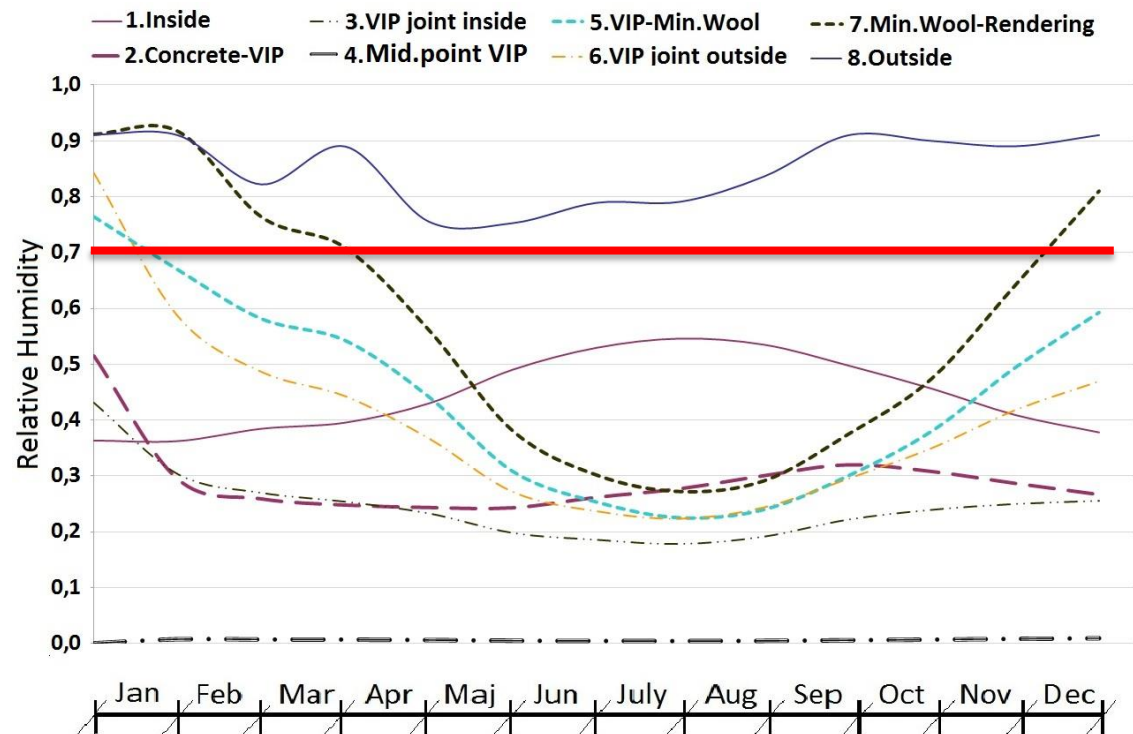
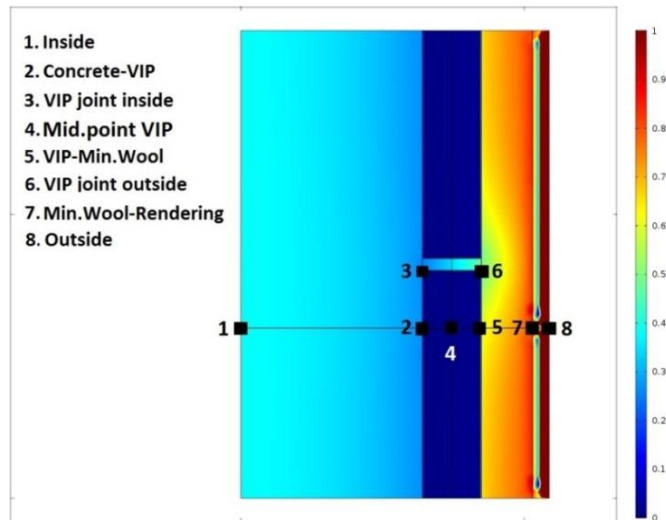
ALL DIMENSIONS IN MM

Simulated heat transport



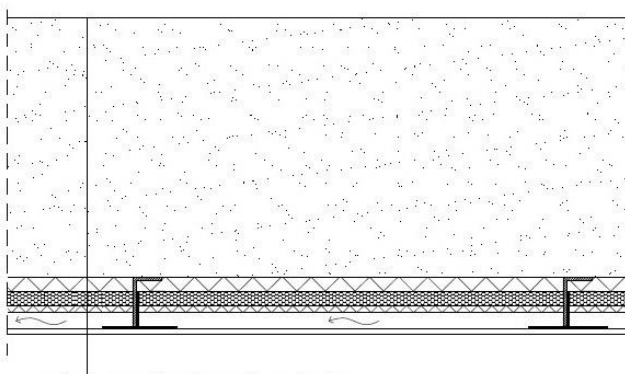
Moisture transport

The relative humidity distribution in wall construction in the long term, extreme conditions.



A new VIP mounting system

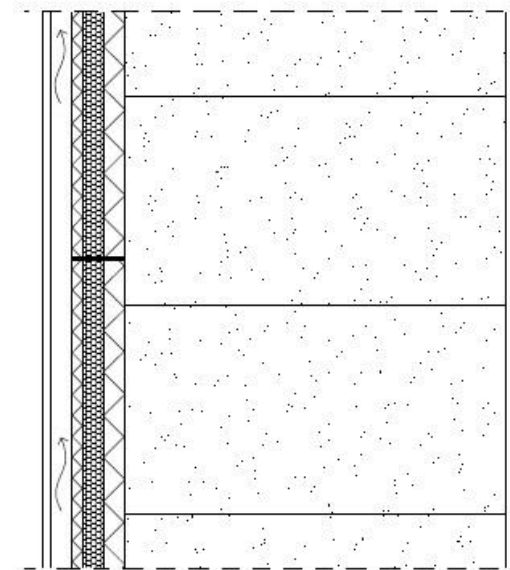
- *Facade components are standard and available at market.*
- *The VIP sandwiches were glued to the outside of the wall structure, by the means of an adhesive (hydraulically setting mortar)*
- *A 3 mm thick L-profile plus a T-profile (stainless steel) provides a flexible ventilating air gap between the façade board and the structure*



Facade system (Horizontal section)

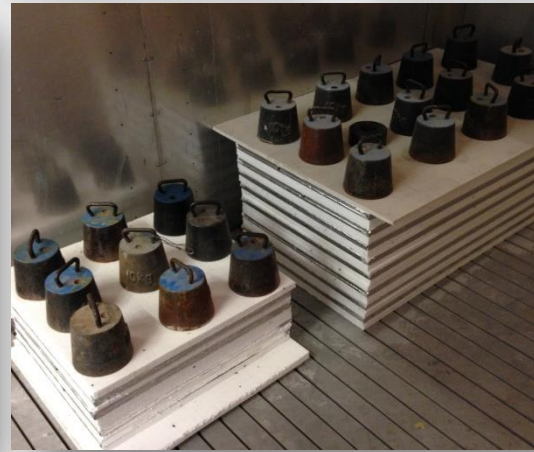
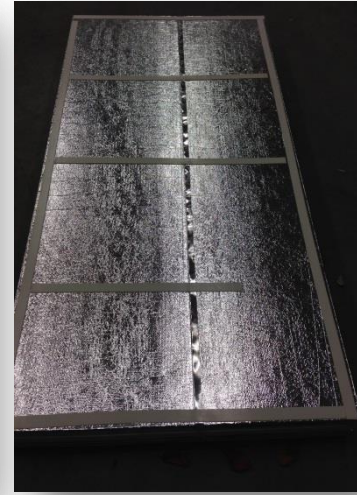
365 mm Light aggregate concrete
 20 mm EPS-Panels
 20 mm Vacuum Insulation Panels (VIPs)
 10 mm EPS-Panels

 70 mm L-Shaped stainless steel sheet
 20 mm Airgap
 12 mm Facade boards
 3 mm Rendering

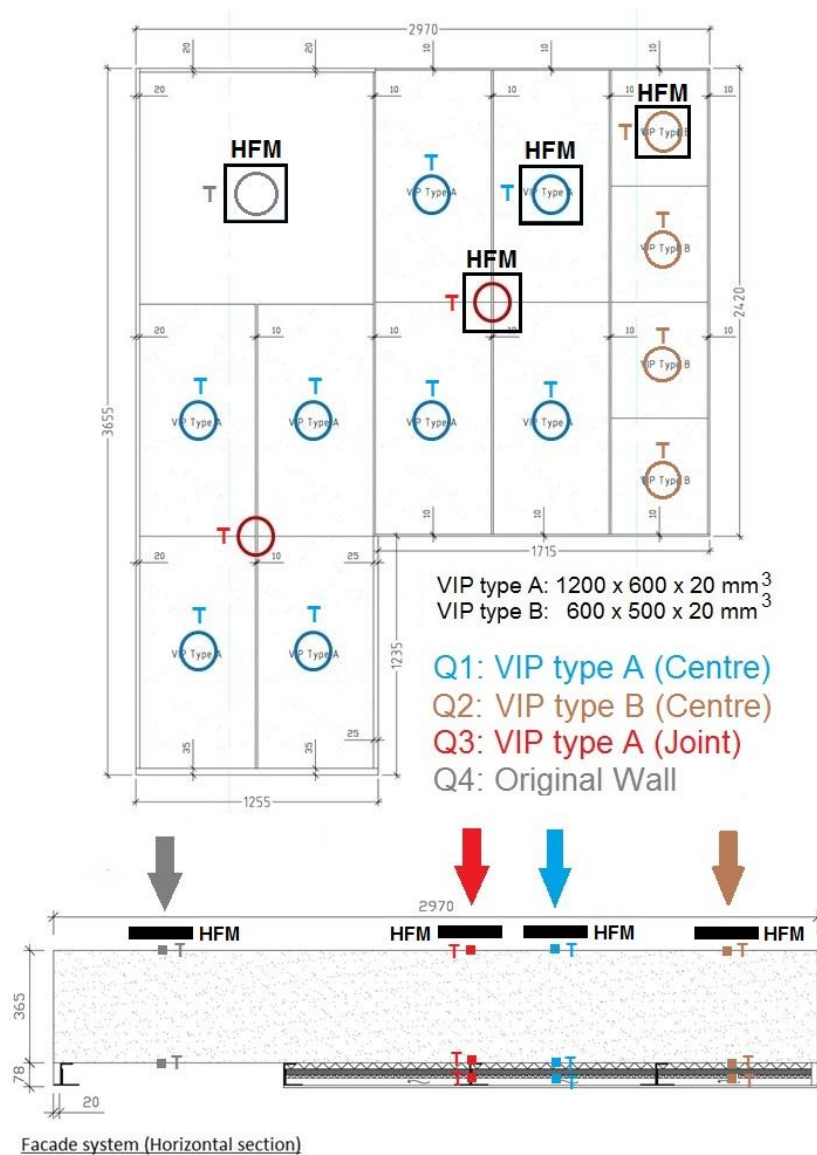


Vertical section

Full scale laboratory measurement



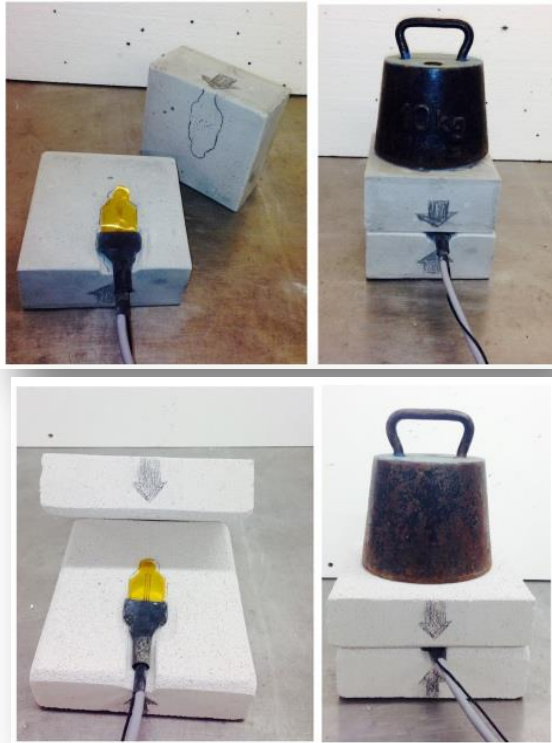




- The heat flow meter (HFM) sensors were mounted in different positions on the interior surface
- 80 temperature sensors, Copper/Constantan as well as Chromel/Alumel thermocouple were installed at various coordinates in the plane of the wall and at the material layer boundaries

Calculated centre-of-panel U-value

The TPS technique (TPS 2500S-ISO/DIS 22007-2.2) used to evaluate the thermal properties of the materials used in the wall



Material	d (mm)	λ (W m ⁻¹ K ⁻¹)	Standard deviations	Source	R (m ² K W ⁻¹)
Aerated concrete blocks	365	0.118	±0.000223	TPS	3.09
Hydraulically setting mortar	2	0.959	±0.000234	TPS	0.002
EPS	20	0.0329	±0.0000156	TPS	0.608
VIP _{centre}	20	0.0042	-	Manufacturer	4.76
EPS	10	0.0329	±0.0000156	TPS	0.304
R _{si}	-	-		Standard value	0.14
R _{se}	-	-		Standard value	0.04
R _{wall}	-	-		-	8.944
Calculated U-value (W m ⁻² K ⁻¹)				Before retrofitting	0.305
				After retrofitting	0.112

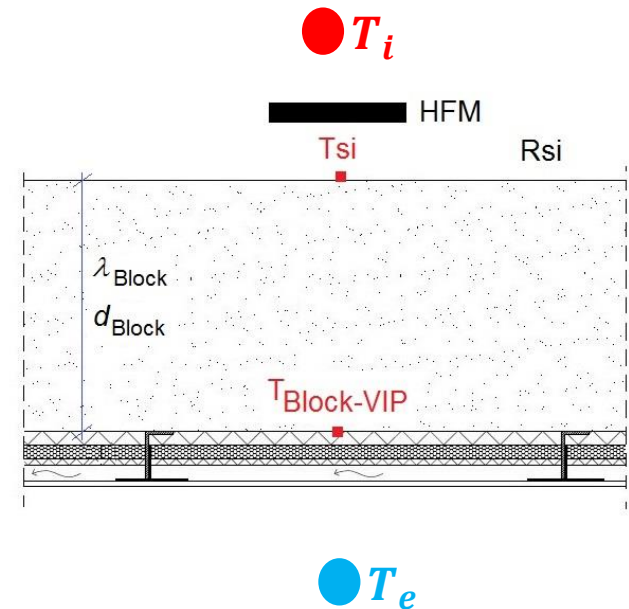
Measured Centre-of-Panels U-value

Centre-of-Panels U-value using Thermocouples and reference material

$$\frac{\lambda_{Block}}{d_{Block}} (T_{si} - T_{Block-VIP}) = U_{wall} (T_i - T_e)$$

Centre-of-Panels U-value by using Thermocouples and HFM sensors

$$\frac{(T_i - T_{si})}{R_{si}} = q_{HFM} = U_{wall} (T_i - T_e)$$



Measured effective U-value

Effective U-value by thermography investigations

$$q_{tot} = U_{centre-of-panel} \cdot \Delta T + \Psi \cdot \frac{P}{A} \cdot \Delta T$$

$$\frac{\frac{T_e - T_{se,VIPcentre}}{R_{se}}}{\frac{T_e - \overline{T_{se}}}{R_{se}}} = \frac{U_{centre-of-panel} \cdot (T_i - T_e)}{U_{effective} \cdot (T_i - T_e)}$$

T_e : Outside air temperature

T_i : Inside air temperature

$\overline{T_{se}}$: Average outside wall surface temperature

$T_{se,VIPcentre}$: Outside wall surface temperature at coordinate of the centre-of-panel

R_{se} : Wall surface thermal resistance at exterior side

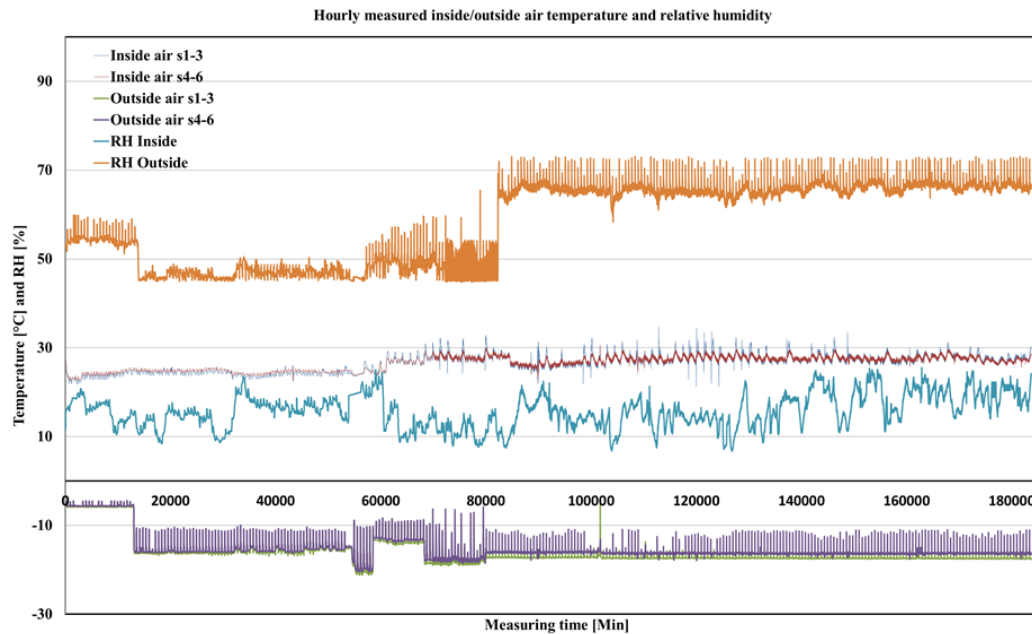
$U_{centre-of-panels}$: Thermal transmittance of the wall at coordinate of the centre-of-panels

$U_{effective}$: Effective thermal transmittance of the wall

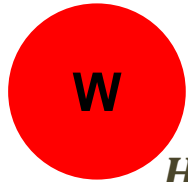


Climatic Condition

Climate sequences	Measuring time (Hours)	Colder side		Warmer side	
		T_e (°C)	RH_e^a (%)	T_i (°C)	RH_e^a (%)
Climatic time sequence No.1	410	-5		22-24	
Climatic time sequence No.2	860	-15	45 – 73	23-28	6.7–25.5
Climatic time sequence No.3	2030	-20		23-28	



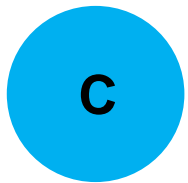
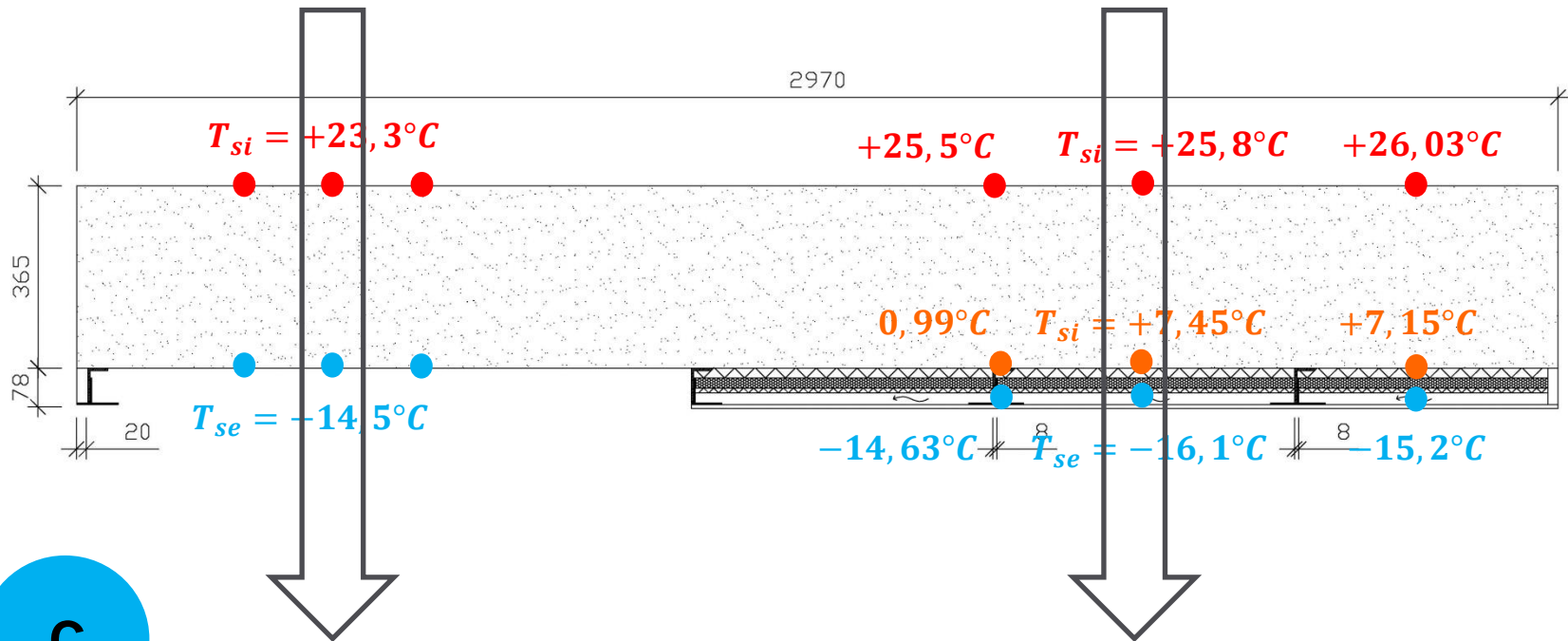
Measured temperatures



● $T_i = +27,63^{\circ}\text{C}$

Heat Flow Meter 2

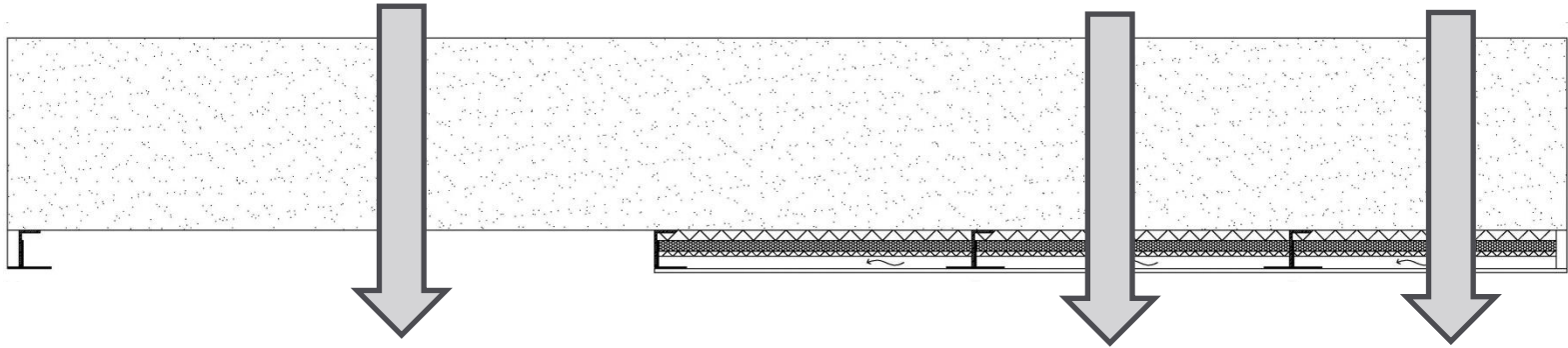
Heat Flow Meter 1



● $T_e = -17,06^{\circ}\text{C}$

Centre-of-Panels U-values

$$R_{si} = 0,24 (m^2 \cdot K)/W$$



Calculated:	0.305	0,112	$W/(m^2 \cdot K)$
Measured: (T-sensors)	0.275	0,121 – 0.136	$W/(m^2 \cdot K)$
Measured : (HFM)	0.323	0,17	$W/(m^2 \cdot K)$

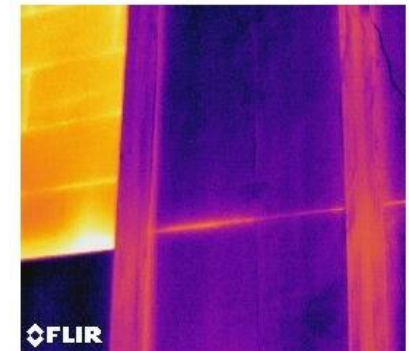
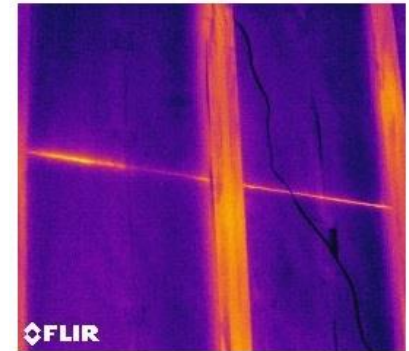
Taking into account an addition standard thermal resistance of a ventilated air gap

Calculated:	0.29	0,109	$W/(m^2 \cdot K)$
Measured: (T-sensors)	0.26	0,118 – 0.132	$W/(m^2 \cdot K)$
Measured : (HFM)	0.3	0,165	$W/(m^2 \cdot K)$

Effective U-value

Measured temperatures:

Placement	VIP No. 5-8	
	VIP _{centre} 1200 × 600 mm ²	VIP _{joint} 1200 × 600 mm ²
Inside air temperature (° C)	28.83	
Interior surface temperature(° C)	25.62	25.52
Concrete blocks -VIP(° C)	6.89	0.58
Exterior surface temperature(° C)	-15.31	-13.31
Outside air temperature (° C)	-16.87	



A comparison of the U-values and λ -values:

	[W/(m ² ·K)]		[mW/(m·K)]
Calculated U _{centre-of-panel}	0,112	According to manufacturer $\lambda_{\text{centre-of-panel}}$	4,2
Measured U _{centre-of-panel}	0,132	Measured $\lambda_{\text{centre-of-panel}}$	≈7
Measured U _{effective}	0,154	Measured $\lambda_{\text{effective}}$	≈10,9

Conclusions

- *Use material with relatively low thermal conductivity at the joints have a significant impact on the resulting U value.*
- *Thermal conductivity of the adjacent insulation next to the VIP's have a measurable effect on the heat flow, while the choice of materials for the mounting (e.g. screws) have a smaller effect on the resulting U value compared to the effect of the material in the joints and adjacent insulation.*
- *Relative humidity calculation shows that the location of the VIP on the outside does not a moisture problem to the construction.*
- *There is no risk of high relative humidity at the joints.*
- *VIPs is a very competitive solution to renovate the construction of the Swedish "Million Program".*
- *This study demonstrates a robust, effective, simple and fast system for external mounting of the VIPs, an improved centre-of-panels thermal transmittance of the wall, in the range of 0.118-0.132 $W m^{-2}K^{-1}$ as well as a low effective thermal conductivity for the VIPs of 10,9 $mW m^{-1}K^{-1}$, are reached.*



Thanks for your kind attention!