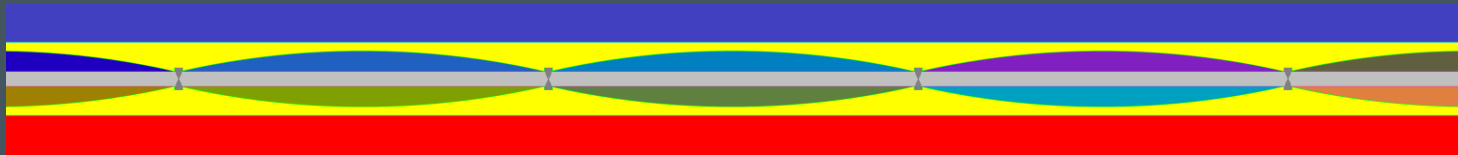


Shallow Hollow Core Vacuum Panels Based on Tied Arch Skins

Design development of a novel building cladding panel using vacuum technology

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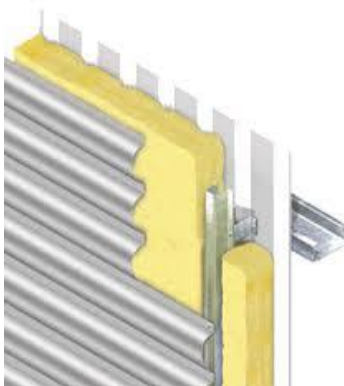


Introduction: Content

- Background (1): why use a vacuum cladding in buildings?
- Background (2): limits of conventional VIP cladding
- Design development: the concept, and challenges to be overcome.
- Design approaches: modelling, analysis and results.
- Next steps: prototyping and production.

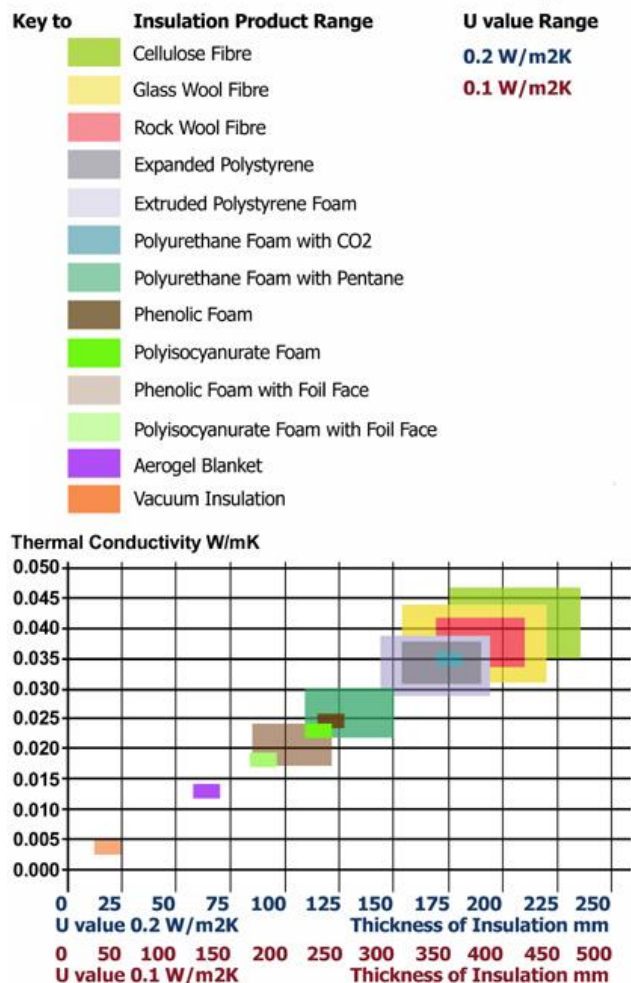
Background: why use vacuum cladding?

- Increasing demand for highly performing building cladding systems: Engineered building components; build off-site; prefabrication; structural cladding (floor-floor)
- Low U-values ($< 0.1 \text{ W/m}^2\text{K}$) / high R values (> 10) for approaching zero carbon buildings as a response to man-made climate change.
- Thinner panels: increased rentable floor space or more dwellings per unit area; reduced mechanical problems (lower self-weight, smaller fixings, lighter building structure)
- Lower embodied carbon in the building envelope as less material is used, and the panels are smaller, lighter and cheaper to transport.



Background: why use vacuum cladding?

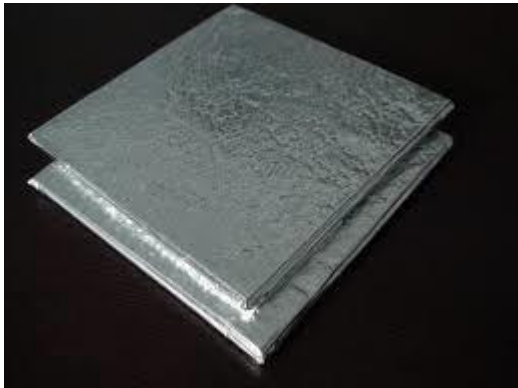
Insulation Thicknesses for U values W/m²K



Source: Audacity.org

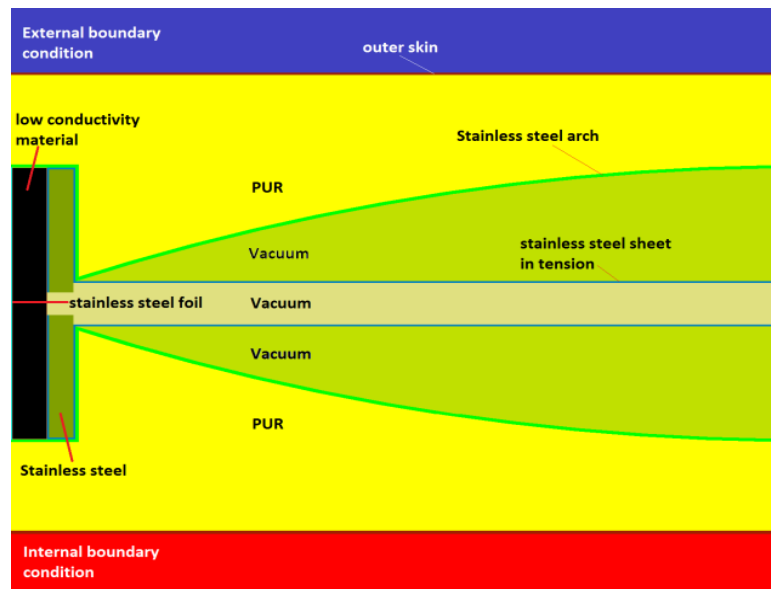
Background: limits of conventional VIP cladding

- Durability during storage, transport, and the building phase: susceptible to mechanical damage and consequent loss of thermal properties.
- Lifespan may not reach more than 30 years: building panels should last at least 60 years before replacement.
- Thermal bridging through the panel junctions and encapsulating barrier film can significantly affect the U-value achieved.
- Alternative approaches such as foam encapsulation of VIPS and evacuated spheres introduce more thermal conduction paths



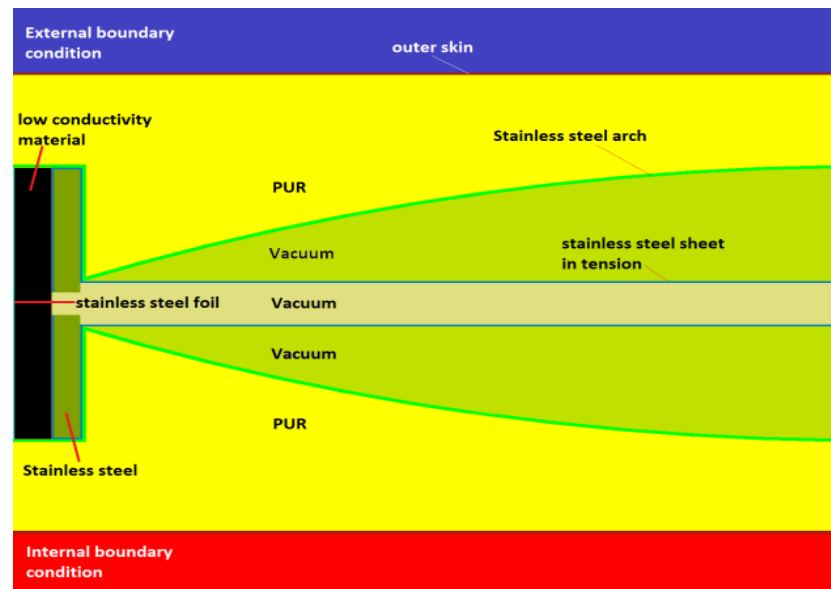
Design development: the concept

- Opposing tied shallow arches of thin stainless steel, held in shape by stainless steel foil under tension.
- Polymeric foam around the assembly protects the panel and provides additional insulation where required (junctions)
- Edge detailing is crucially important to maintain thermal performance



Design development: design criteria

- Largest possible panel size to maintain a favourable area to edge ratio
- Stainless steel to avoid contamination of the vacuum, thickness <0.7mm
- U-values of 0.11 – 0.09W/m²K
- A nominal panel thickness of 115-140mm



Design development: Structural assessment

- Panels must resist atmospheric pressure of approximately 10 tonnes/m²
- Arch configuration make use of thin gauge steel possible.

Key design issues:

- Geometry of the arch (span, height)
- Gauge and profile of steel used

The height-width ratio is critical – if the arch is too shallow, bending and shear dominate.

Second order elastic analyses were undertaken for a height of 50mm at various widths using an un-profiled skin

Design development: Structural assessment – flat steel

| Width | Tie thickness (mm) | Skin thickness (mm) | Inertia (mm ⁴ /m)* |
|------------|--------------------|---------------------|-------------------------------|
| 600 | 0.43 | 3.73 | 4325 |
| 500 | 0.3 | 2.92 | 2075 |
| 400 | 0.19 | 2.2 | 887 |
| 300 | 0.11 | 1.54 | 304 |
| 200 | 0.05 | 0.95 | 71 |
| 150 | 0.03 | 0.71 | 30 |
| 100 | 0.02 | 0.50 | 10 |

Skin has to be very thick to withstand the stresses at 600mm when un-profiled (flat) steel is used

Design development: Structural assessment – ribbed steel

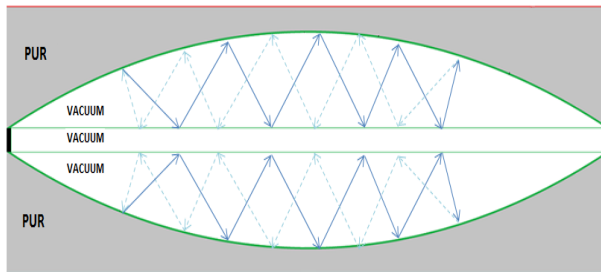
- Profiled steel (ribbed) was considered, of 200mm, 100mm, 50mm and 20mm spacing.
- 200mm and 100mm spacing were susceptible to local buckling and rejected.
- 50mm and 20mm spacing both worked.

Table shows results for
20mm ribs.

| Rib height (mm) | Suitable arch width (mm) | | | |
|-----------------|--------------------------|------------|------------|------------|
| | 0.7mm skin | 0.6mm skin | 0.5mm skin | 0.4mm skin |
| 1 | 200 | 200 | 200 | 200 |
| 2 | 300 | 300 | 300 | 300 |
| 3 | 400 | 400 | 400 | 400 |
| 4 | 500 | 500 | 500 | 400 |
| 5 | 600 | 500 | 500 | 500 |
| 6 | - | 600 | 600 | 500 |
| 7 | - | - | - | 600 |

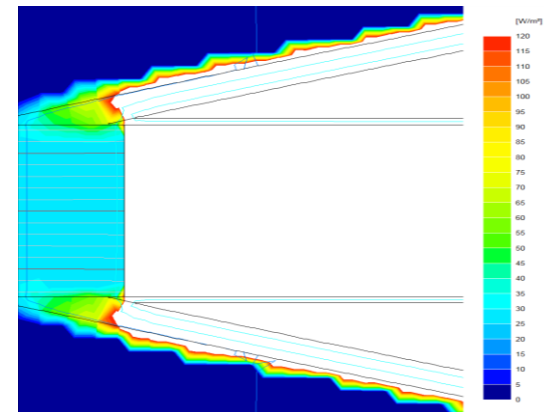
Design development: Thermal assessment

- Heat transfer through the panel is 15-20% radiative and 80-85% conductive
- Radiative heat transfer minimized by use of six low emissivity surfaces (shiny stainless steel)



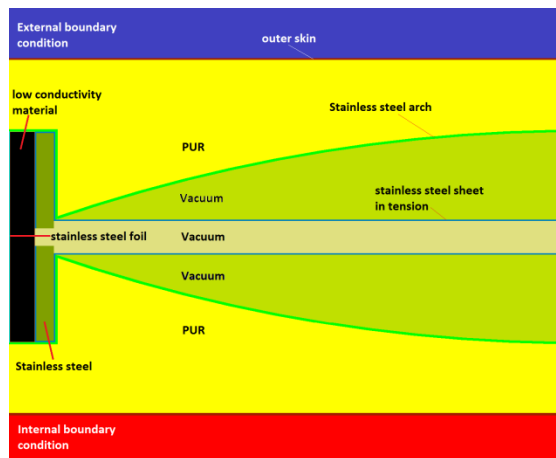
Physibel modelling (BISCO):

Conduction occurs along the panel skins and through the edge detail. Edge detail design is critical



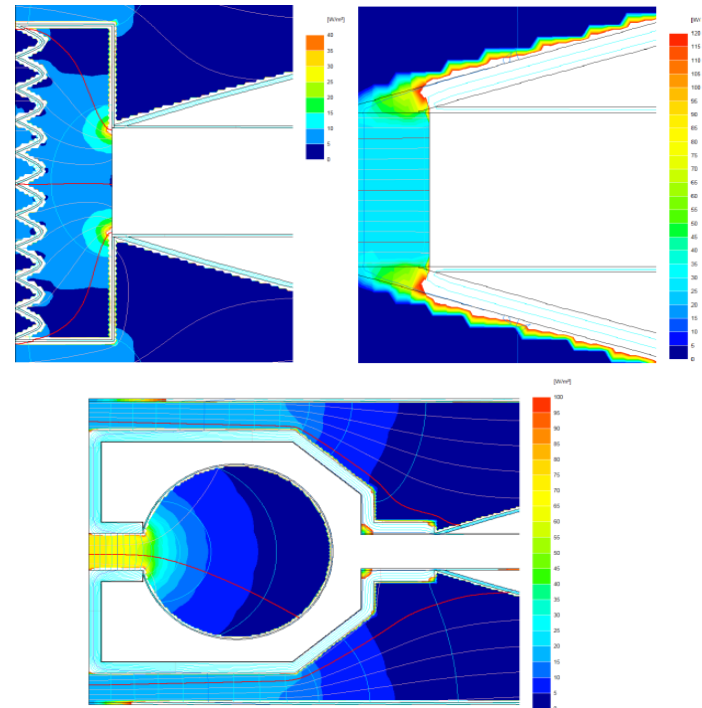
Design development: Thermal assessment

- Thermal engineering of edge detail to keep edge losses to a minimum.
- Conduction is the main heat flow mechanism:
 - External panel face to foam fill
 - Foam to arch and arch edge detail
 - Edge detail to foil through stainless steel and support material
 - Edge detail to edge detail through the load carrying contact points



Design development: Engineered Edge Detail

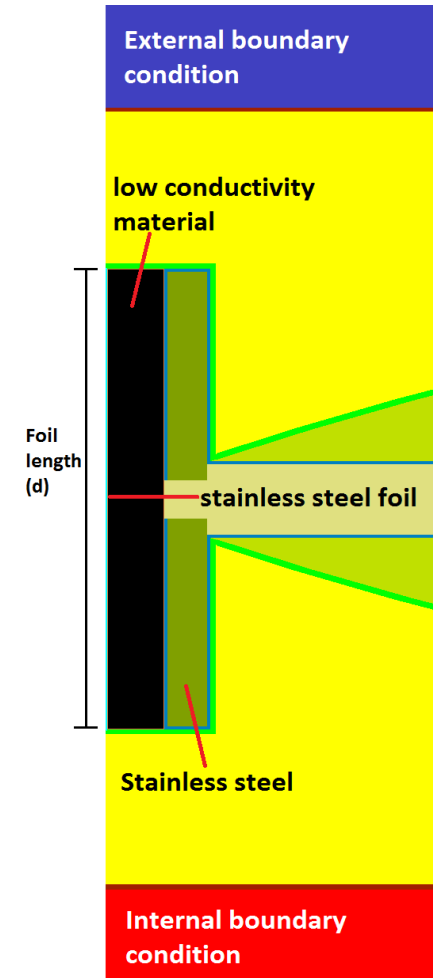
- A variety of edge detail designs were investigated.
- Objective was to maintain vacuum with minimal conduction
- Minimal foil thickness
- Maximum conduction path length



Design development: Engineered Edge Detail

- The final design as chosen:
- 60mm conduction path is required for target U-value

| Foil length (d) (mm) | U-Value without considering the heat loss through the structural elements between arches (W/m ² .K) | Additional heat transfer through the structural elements (W/m ² .K) | Effective U-value (W/m ² .K) |
|----------------------|--|--|---|
| 20 | 0.101 | 0.006 | 0.107 |
| 30 | 0.098 | 0.006 | 0.104 |
| 40 | 0.096 | 0.006 | 0.102 |
| 50 | 0.095 | 0.006 | 0.101 |
| 60 | 0.094 | 0.006 | 0.1 |
| 70 | 0.094 | 0.006 | 0.1 |



Conclusions

- A coreless vacuum panel has been developed and assessed both structurally and thermally.
- A U-value of $0.1\text{W/m}^2\text{K}$ can be achieved with a thickness of 100mm
- Next steps: prototyping to evaluate structural and thermal performance
- High performance building cladding with very low embodied energy