

# Dynamic Simulation of VIP Moisture and Heat Transport

**9th International Vacuum Insulation Symposium**

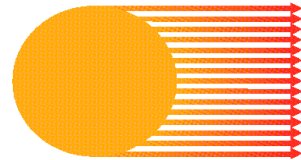
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# Structure



- Motivation
- Measurements of heat and moisture transport
- Description of heat and moisture transport
- Calculations of hygrothermal conditions in VIP
- Conclusion



# Motivation



The increase in thermal conductivity is approximately proportional to the water content

0.5 mW/(mK) per 1 mass-% moisture content  $u$

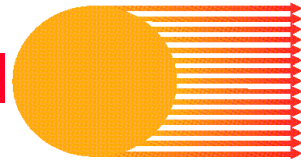
Schwab et al, ZAE Bayern, 2003

Beck et al, HFT Stuttgart, 2006

- How can this be explained?
- What happens within a moist VIP if the temperatures on the boundaries vary?

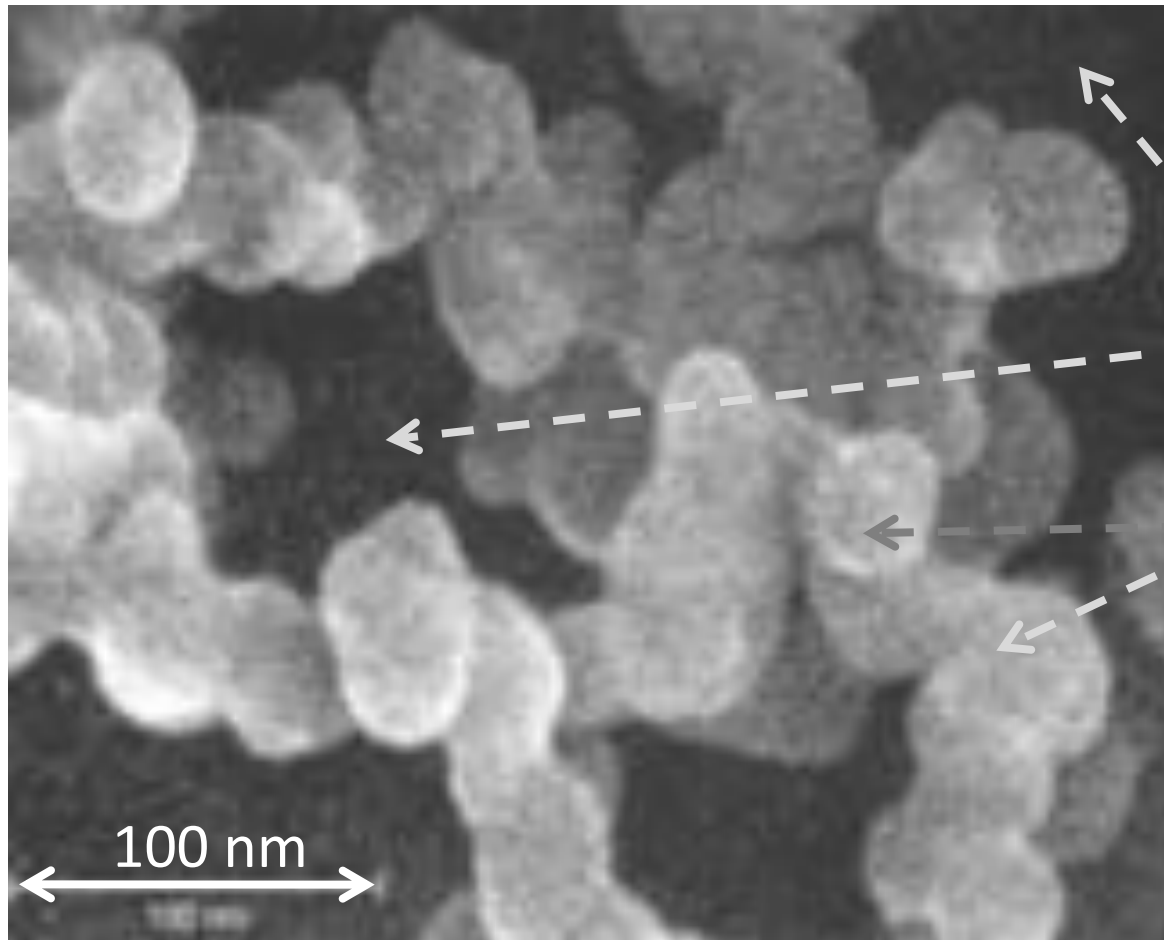


# Microscopic structure of the silica kernel



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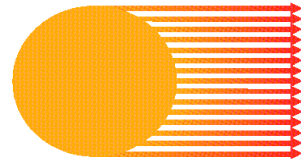
water vapor

adsorbed  
water molecules

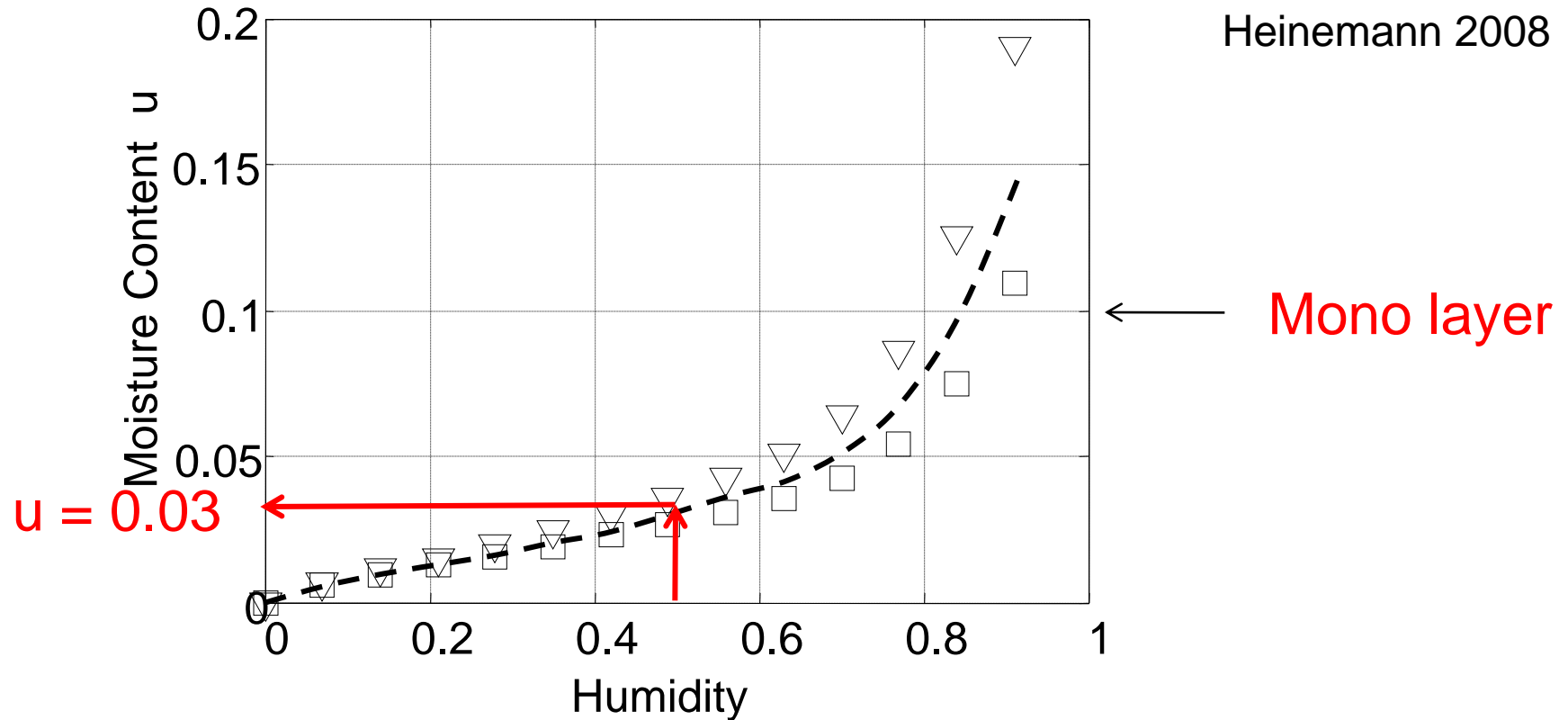
Wacker Chemie



# Sorption Isotherm



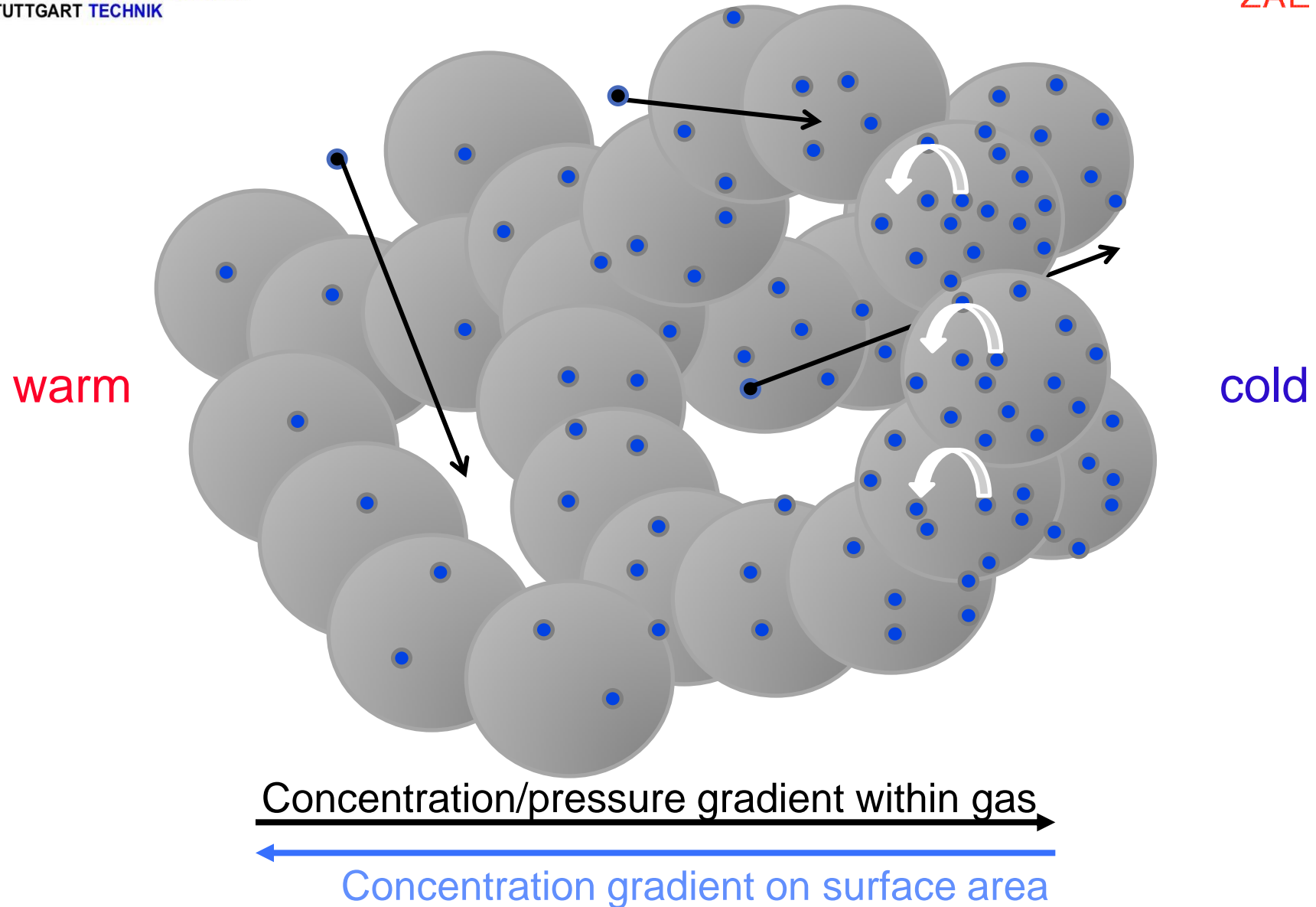
Heinemann 2008



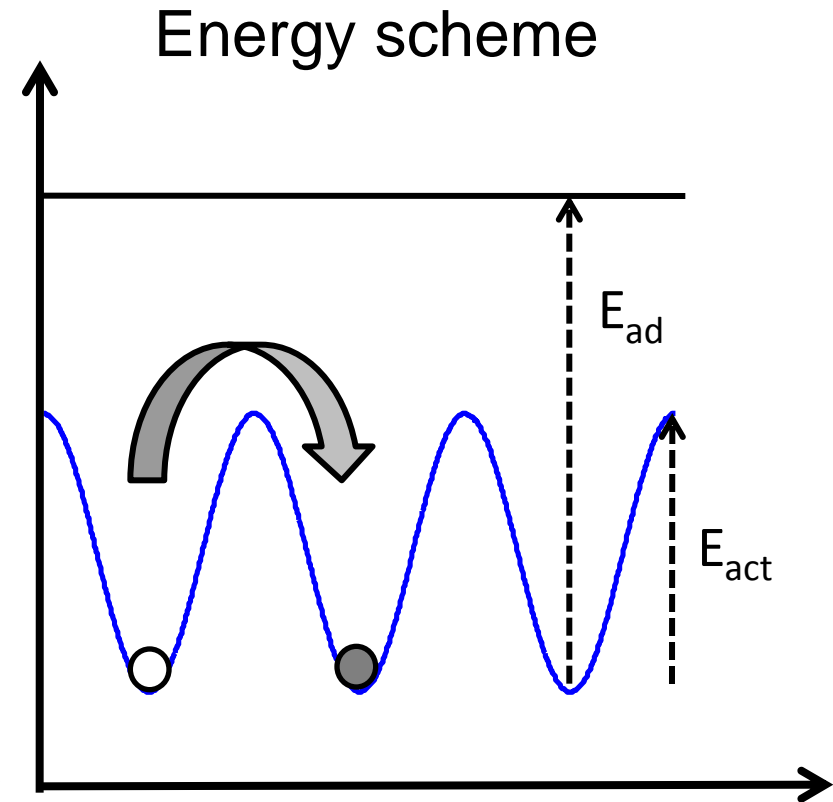
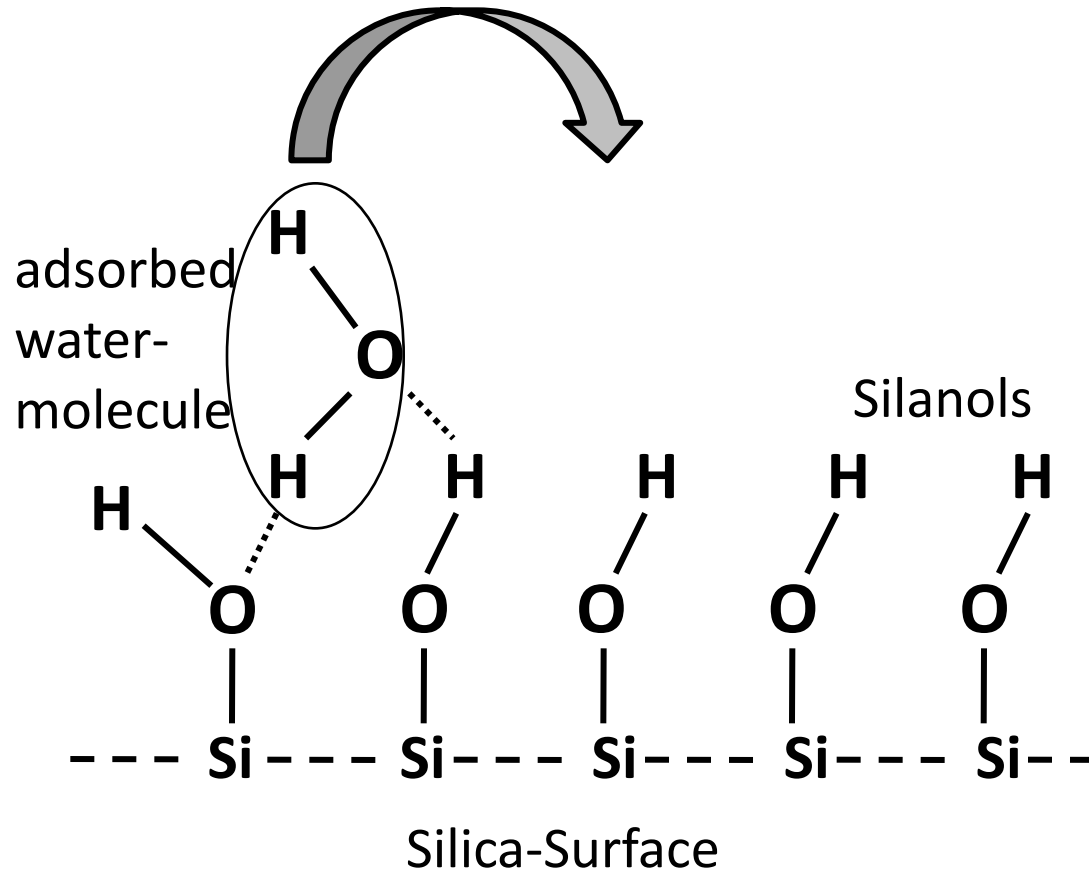
$$u = 0.03 \xrightarrow[\Phi = 0.53 \text{ nm}]{S = 300 \text{ m}^2/\text{g}} \Theta = 30\% \text{ „surface coverage“}$$

Clark 1985

# Surface and bulk diffusion



# Surface migration of adsorbed water molecules



Surface-Location  $x$

$$E_{ad} = 50 \text{ kJ/mol}$$



# Heat and moisture transport



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$$\rho \frac{\partial u}{\partial t} = \frac{\partial}{\partial x} \left\{ \frac{D_K}{RT} \frac{\partial p}{\partial x} + D_s \frac{\partial n_s}{\partial x} \right\} \quad (1) \quad \text{moisture (1)}$$

and

$$\rho c_p \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left\{ \lambda(p) \frac{\partial T}{\partial x} + E_{ad} \frac{D_K}{RT} \frac{\partial p}{\partial x} \right\} \quad (2) \quad \text{heat (2)}$$

transport

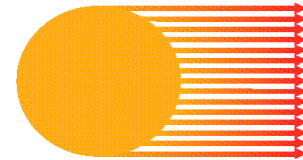
$D_K$  : *molecular* diffusion coefficient

$D_s \sim \exp \left( -\frac{E_{act}}{RT} \right)$  *surface* diffusion coefficient

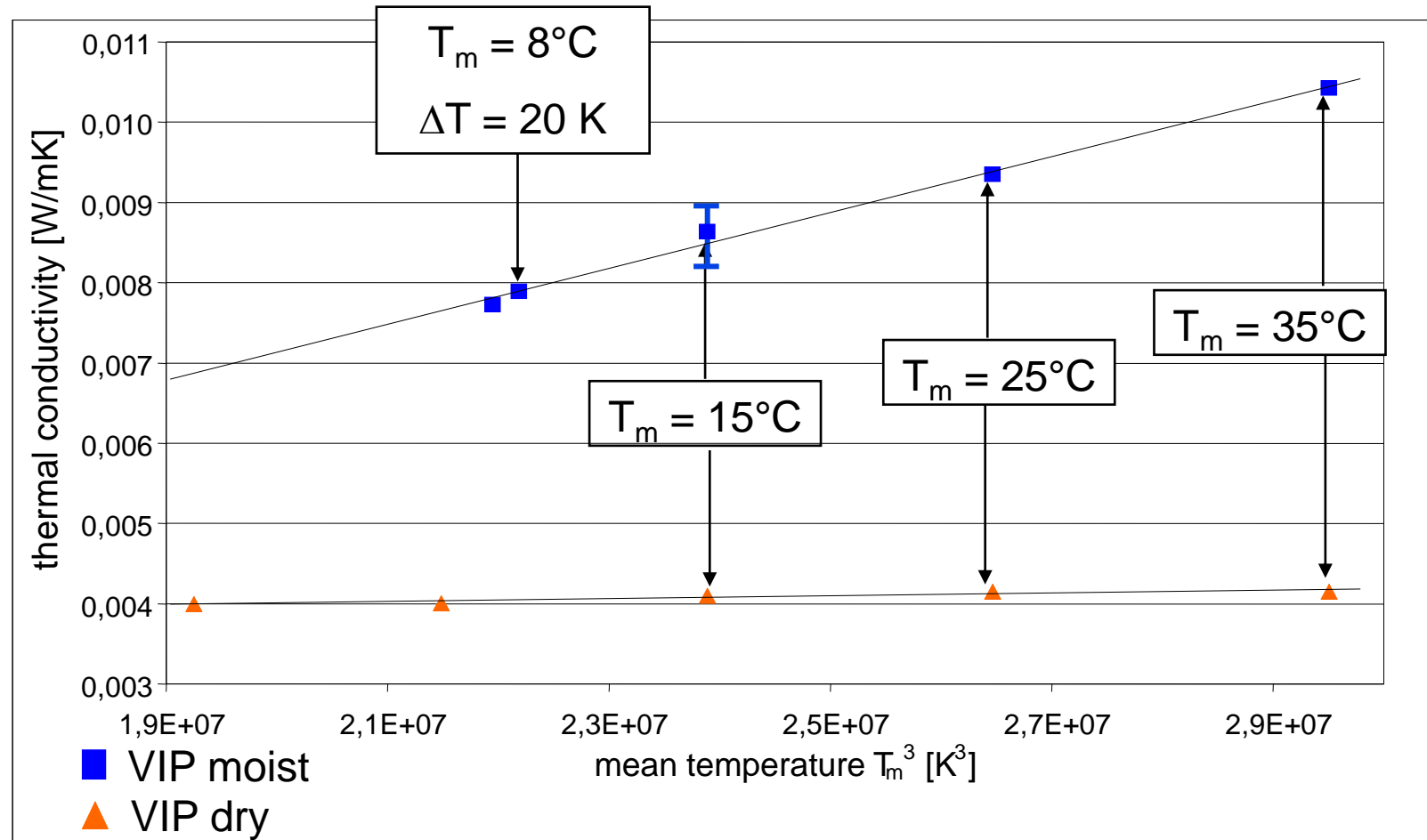




# Dependence of $\lambda$ on temperature for dry and moist VIP ( $u = 4.2 \text{ M-\%}$ )



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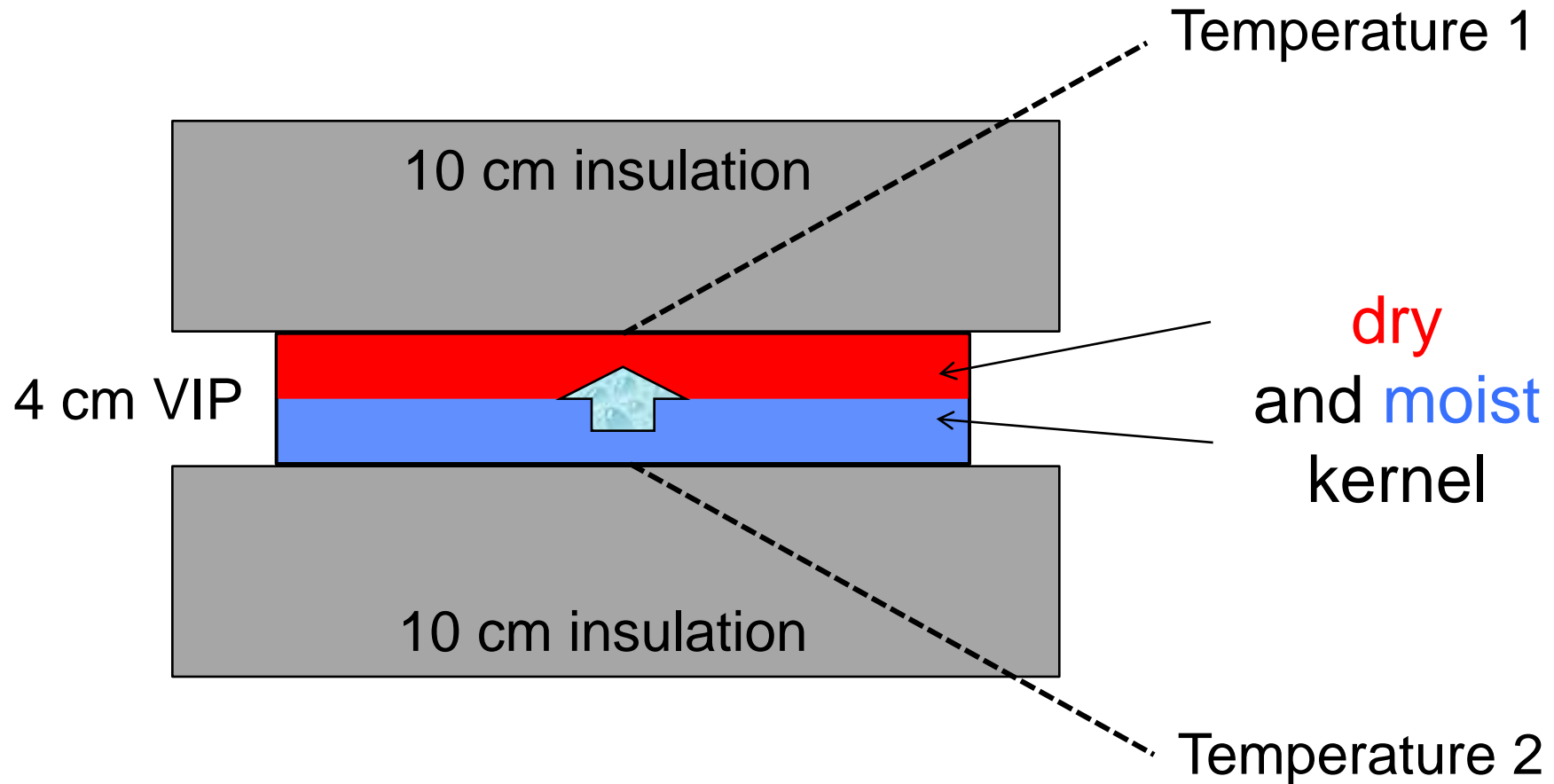
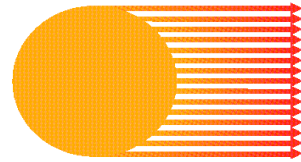


$$E_{\text{act}} = 20 \text{ kJ/mol}$$

Beck 2007

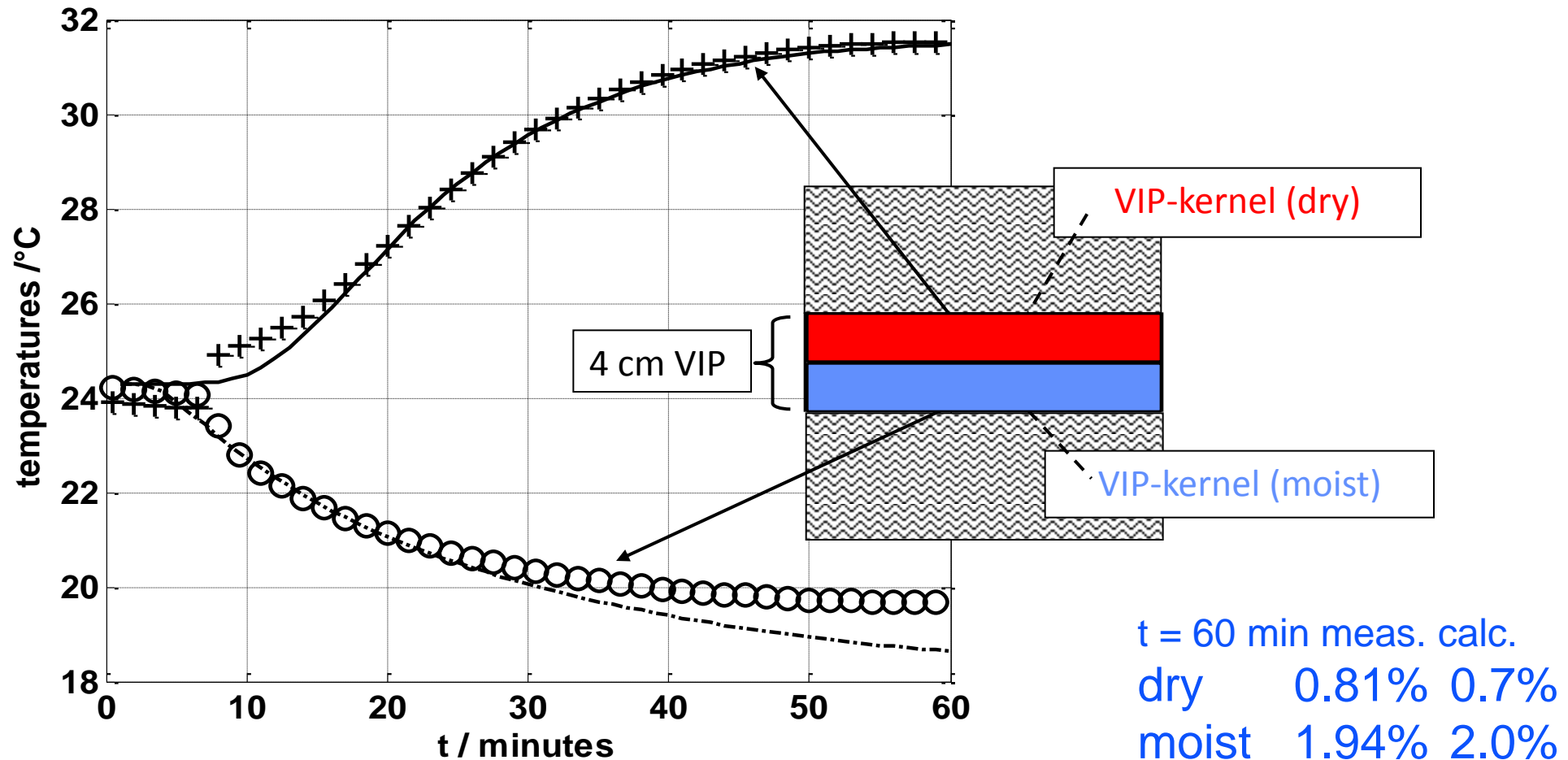
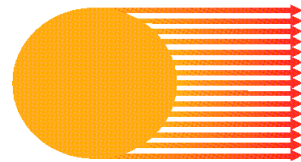


# Experimental Set-up to measure $D_K$





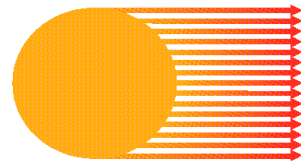
# Temperatures due to de- and adsorption processes within the VIP



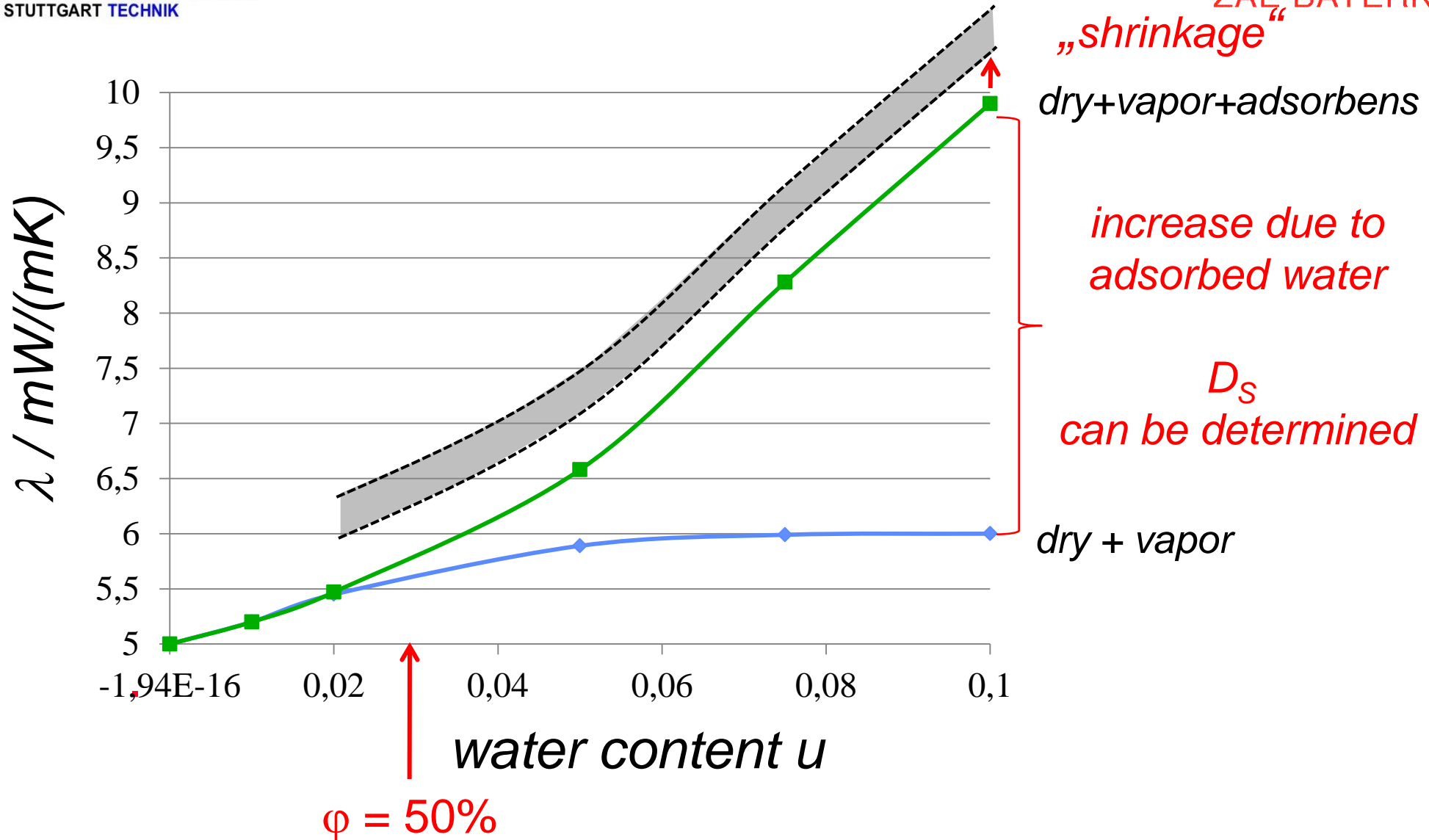
$$D_K = (1.6 \pm 0.2) \cdot 10^{-5} \text{ m}^2/\text{s} \rightarrow d = 100 \text{ nm „pore size“}$$



# Model predictions: Thermal conductivity $\lambda$ versus water content $u$

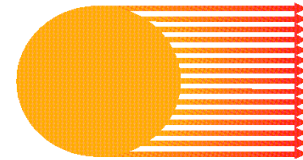


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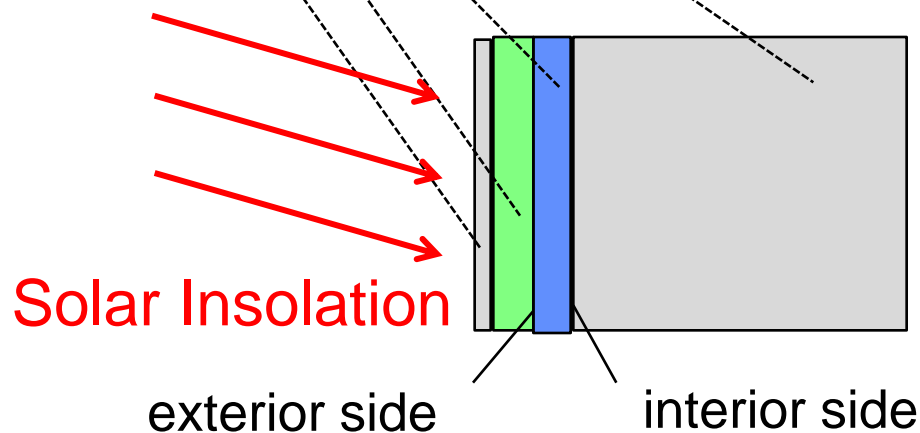


# Hygrothermal conditions within VIP in different wall constructions



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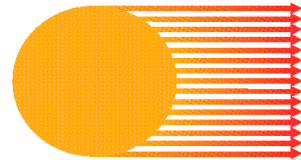
Material	Heat capacity [kJ/(kg*K)]	Thermal conductivity [W/(m*K)]	Density [kg/m <sup>3</sup> ]	Construction #1	Construction #2
				Thickness of layer [m]	Thickness of layer [m]
Brick	1000	0.5	2000	0.30	0.30
VIP	700	Variable	200	0.02	0.02
Additional insulation	1000	0.04	30	0.00	0.02
Plaster	1000	0.8	1000	0.005	0.005



Solar absorption coefficient  
 $a = 0.2$  to  $0.7$

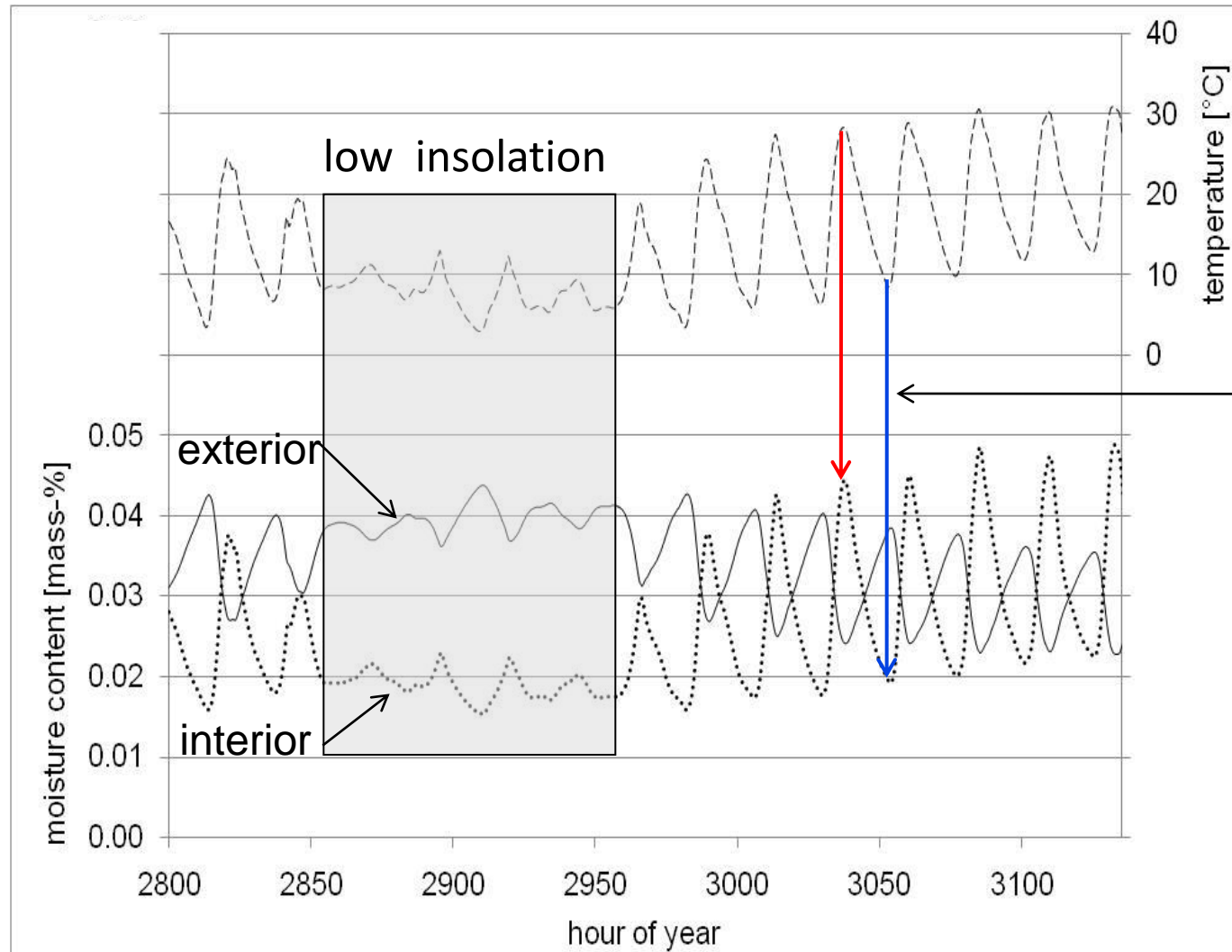


# Moisture migration due to temperature fluctuations (springtime)



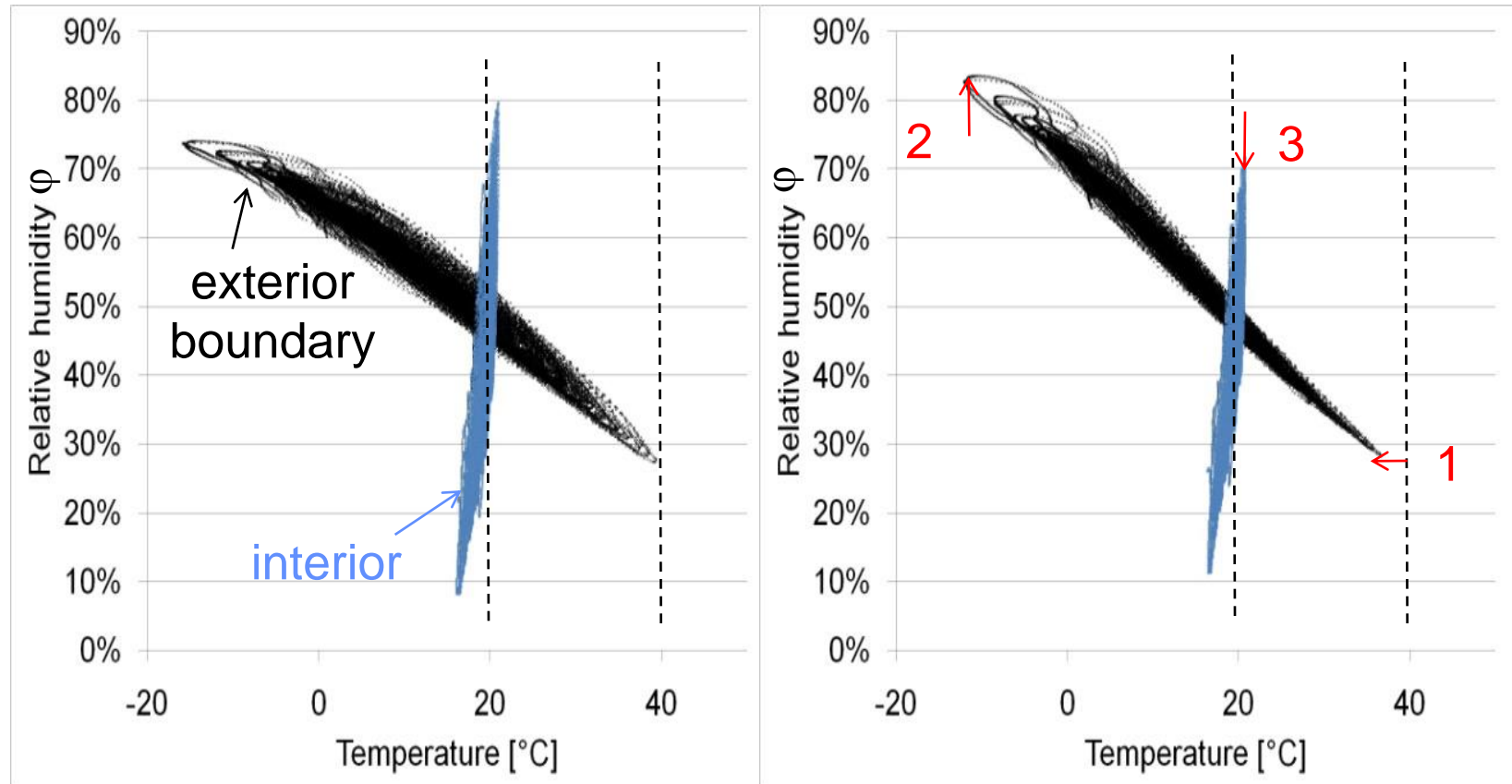
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# Relative humidity versus temperature – without (left) and with insulation (right)

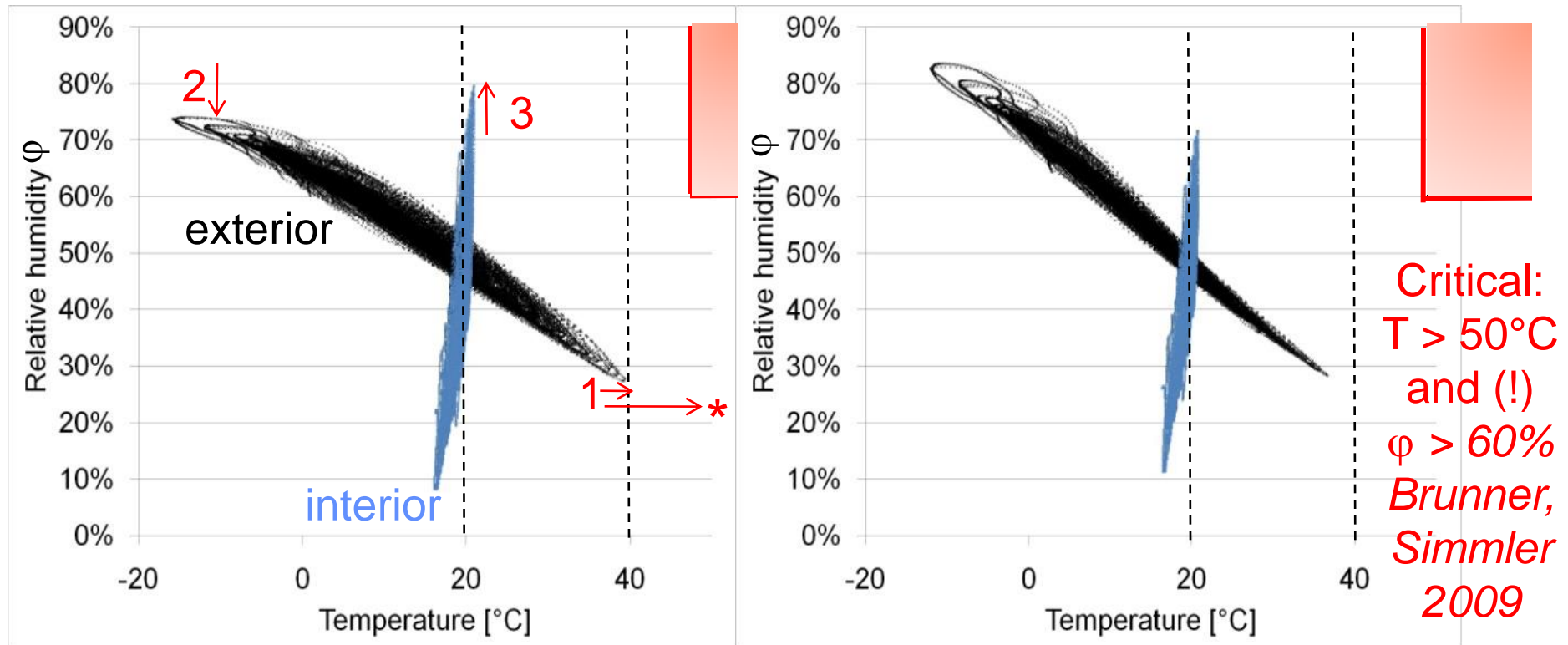
solar absorption coefficient  $a = 0.2$



- 1) decrease of temperature
- 2) increase of humidity by about 10%
- 3) decrease of humidity by about 10%

light wall

massive wall



- 1) increase of temperature
- 2) decrease of humidity by about 10%
- 3) increase of humidity by about 10%

\*  $T_{\max} = 50^{\circ}\text{C}$  for  $a = 0.7$

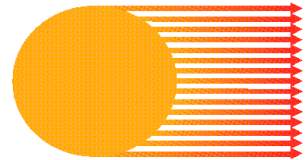




# Summary



- A model was developed and tested to describe the heat and moisture transport within VIP
- The hygrothermal conditions within VIP were calculated quantitatively
- High temperatures (max. 50°C to 60°C; depending on solar absorption, orientation etc.) correspond to low humidity and vice versa
  - total increase of the thermal conductivity due to moisture:  $\Delta\lambda \cong 1 - 2 \text{ mW}/(\text{m K})$
  - no aging of the laminates are expected



Thank you for your attention