

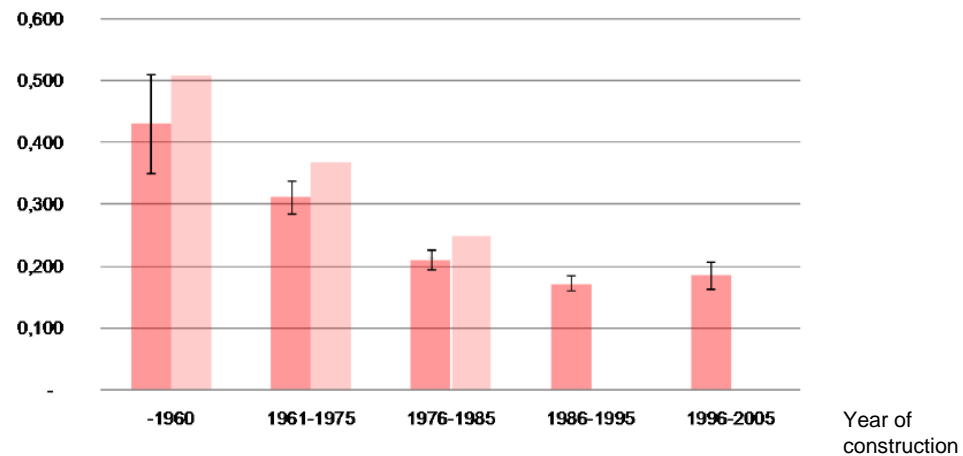


A Parametric study of a metal sandwich VIP

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U-value, W/m²K outer walls, one family houses



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APPROACH

COST

CONCLUSIONS



www.norrlandstrahus.se

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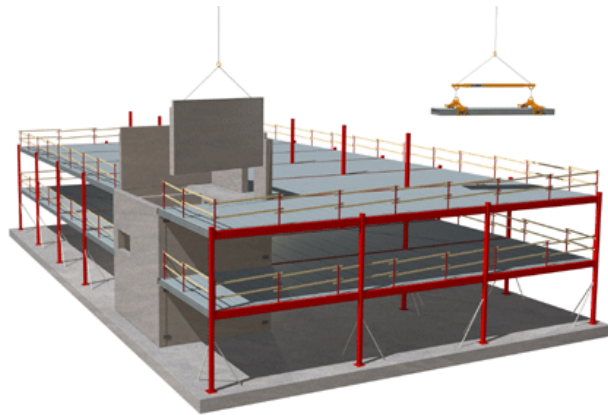
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The Average Swedish one family house

Built in 1953

1,5 floors with a cellar

Wooden facade

$A_{\text{temp}} = 160 \text{ sqm}$

$U_{\text{wall}} = 0,334 \text{ W/m}^2\text{k}$



Foto: Conny Fridh/Johnér

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The Average Swedish Multi Family House

Built in 1959

3 floors with a cellar

Rendered or brick facade

$A_{\text{temp}} = 1426 \text{ sqm}$

17 apartments

$U_{\text{wall}} = 0,411 \text{ W/m}^2\text{k}$



Foto Niklas Almesjö/Bildarkivet.se

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VIP panel

Part of a prefab system

Systematic solutions for Refurbishment

Durability

Mechanical Resistance

(Core materials other than fumed silica)

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Investigate the use of full metal VIPs

Active panels

Focus on Thermal bridge

Cost calculations

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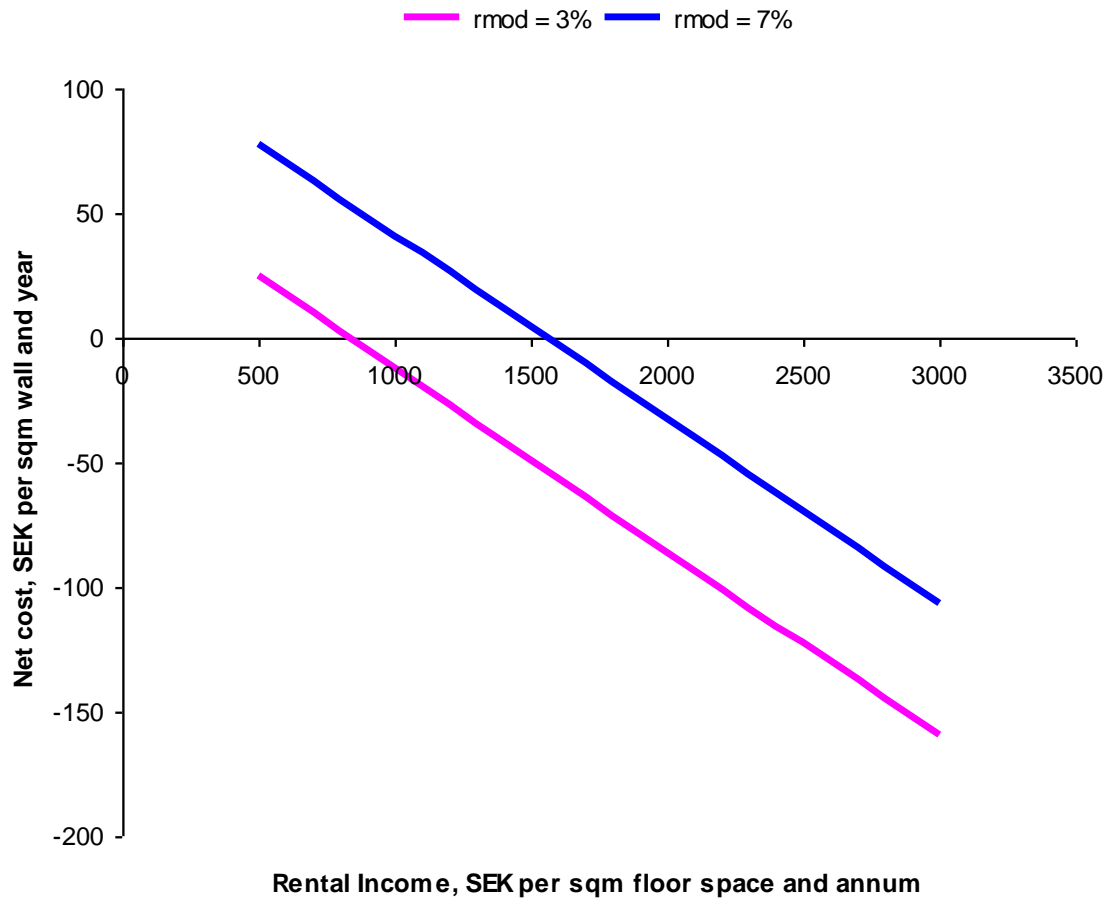
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Period of 50 years

Panel size 600 by 1000 mm

Price of VIP is 1090 SEK per panel

Panel thickness of 30 mm

$\lambda_{\text{centerofcore}} = 0,004 \text{ W}/(\text{m}\cdot\text{K})$

$\psi_{\text{edge}} = 0,01 \text{ W}/(\text{m}\cdot\text{K})$

$\lambda_{\text{traditional}} = 0,04 \text{ W}/(\text{m}\cdot\text{K})$

Price of traditional insulation is 1000 SEK/m³

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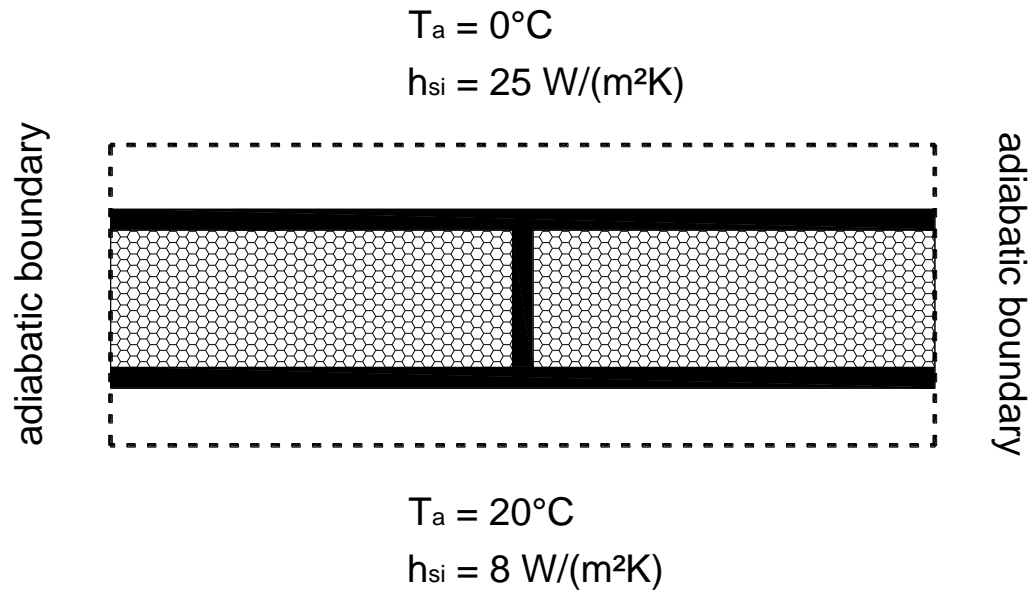
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Thermal bridge

Two dimensional calculation model



representative section, boundary conditions

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Parameters

Material of the envelope

Thickness of cover

External insulation to break thermal bridge

Lengthening of the joint

The effect on the thermal edge loss

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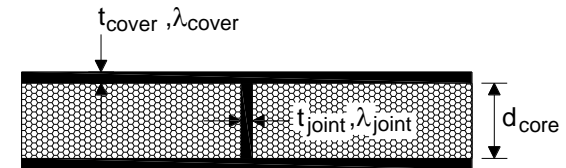
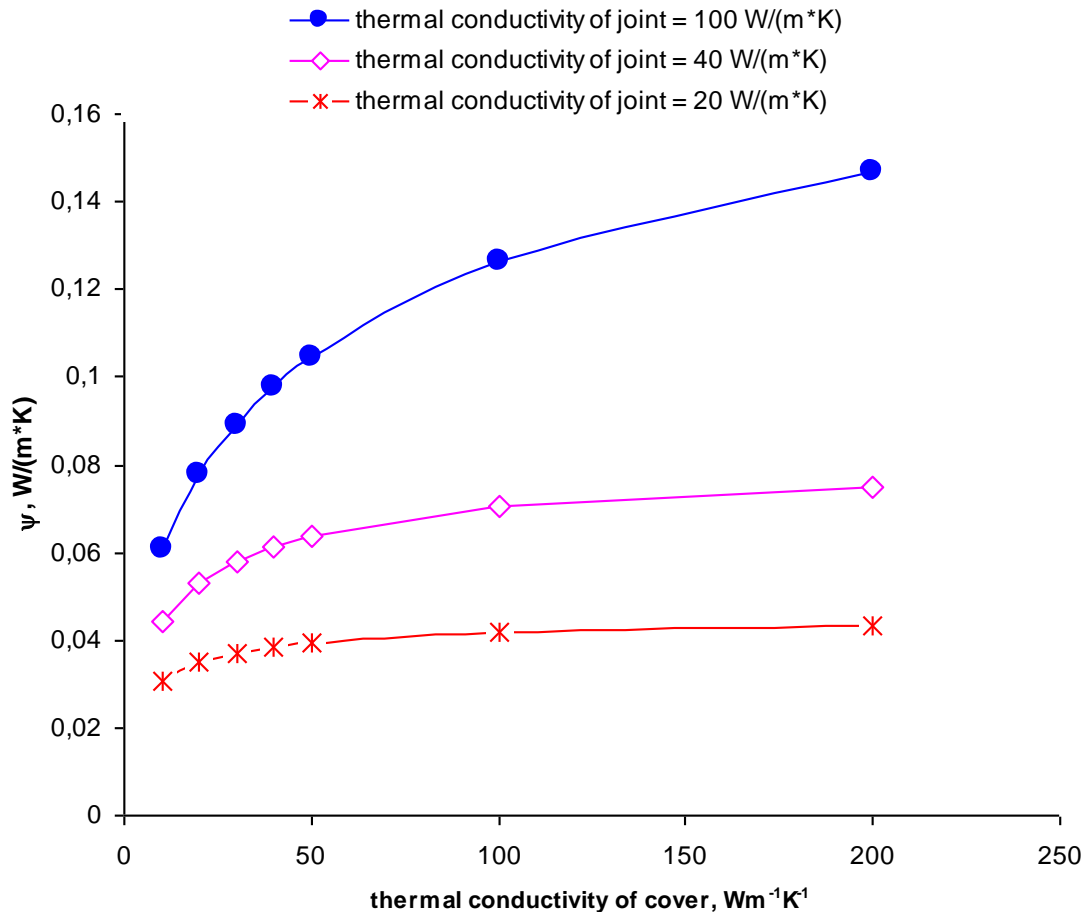
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thermal conductivity of the cover



$$t_{\text{cover}} = 0,05 \text{ mm}$$

$$t_{\text{joint}} = 0,05 \text{ mm}$$

$$d_{\text{core}} = 20 \text{ mm}$$

$$\lambda_{\text{core}} = 0,004 \text{ W}/(\text{m}\cdot\text{K})$$

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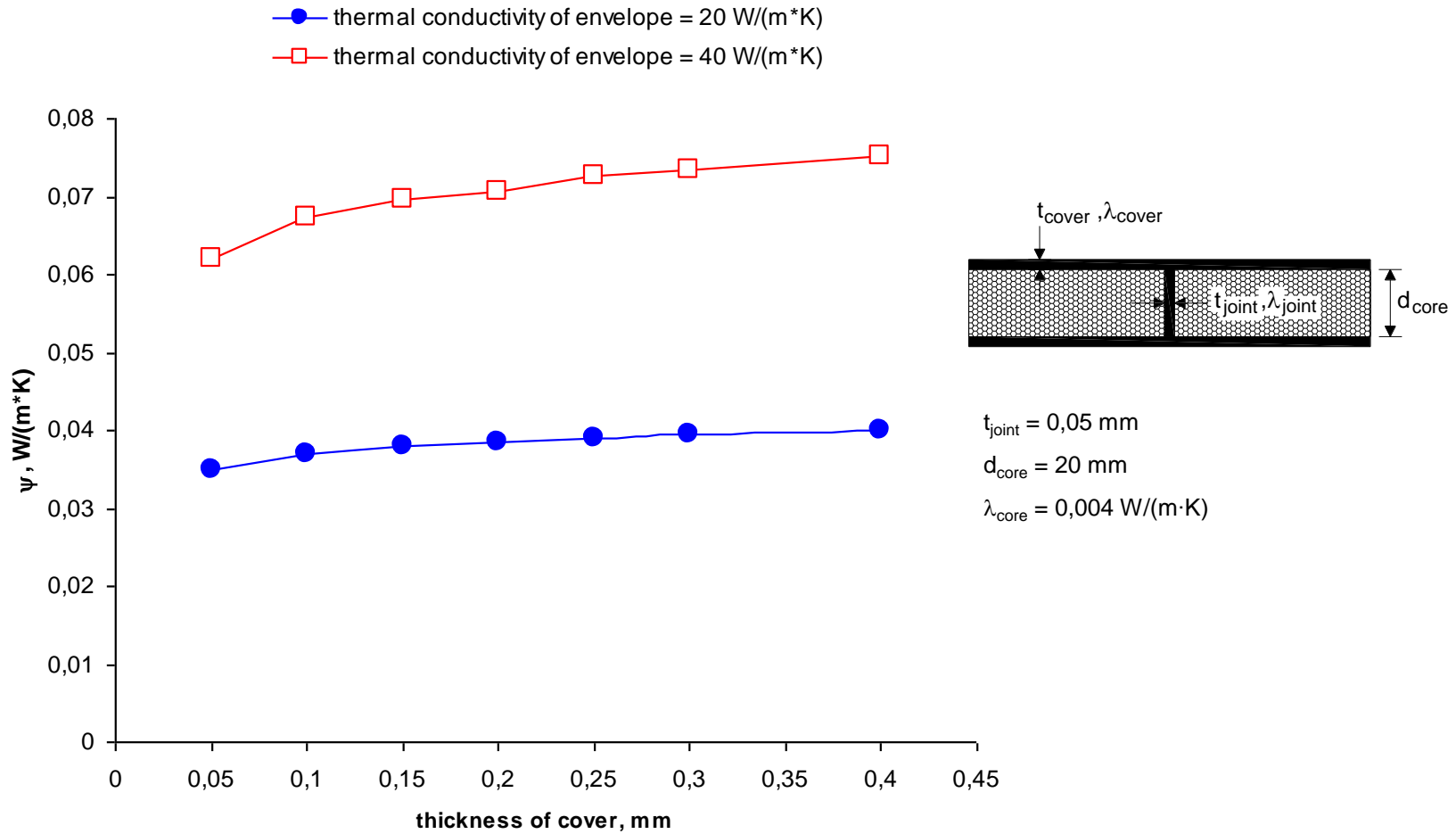
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thickness of cover



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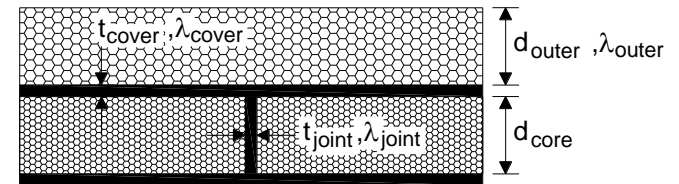
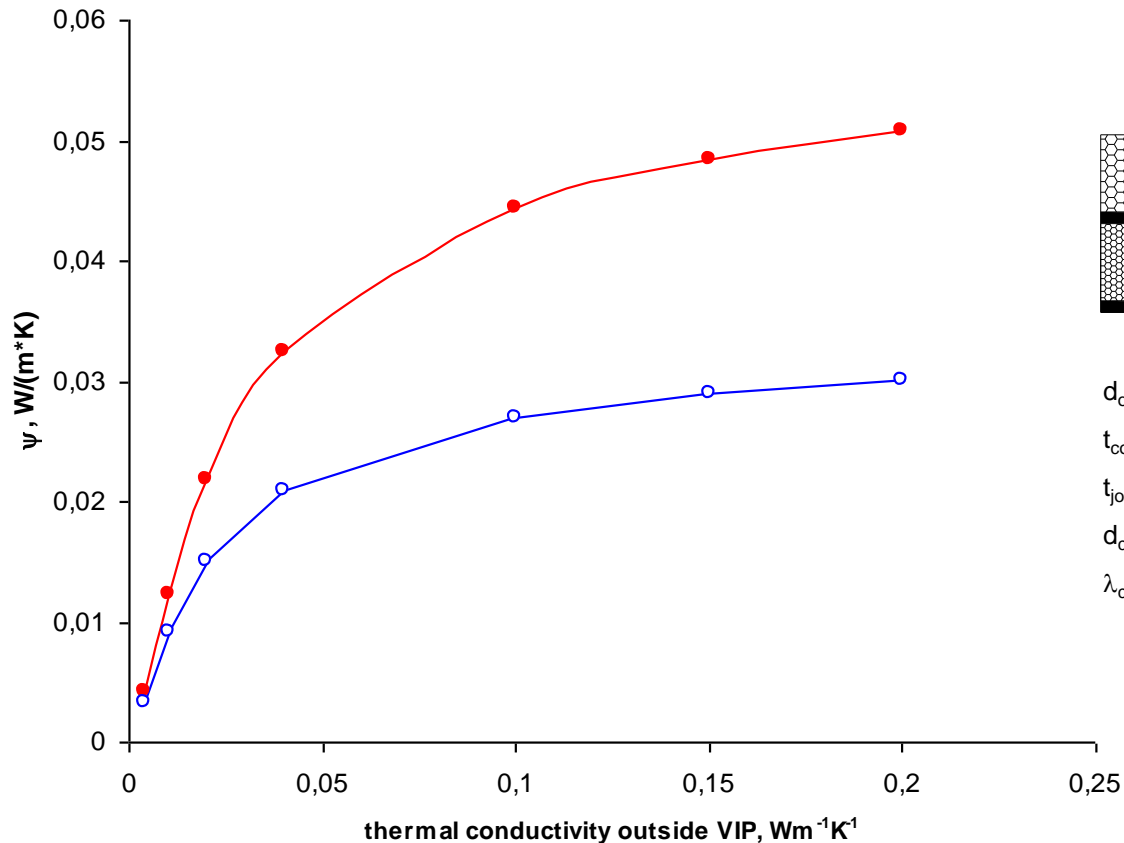
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outside thermal conductivity

- thermal conductivity of envelope = 40 W/(m·K)
- thermal conductivity of envelope = 20 W/(m·K)



$d_{\text{outer}} = 20 \text{ mm}$
 $t_{\text{cover}} = 0,05 \text{ mm}$
 $t_{\text{joint}} = 0,05 \text{ mm}$
 $d_{\text{core}} = 20 \text{ mm}$
 $\lambda_{\text{core}} = 0,004 \text{ W}/(\text{m}\cdot\text{K})$

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Altering the geometry of the joint

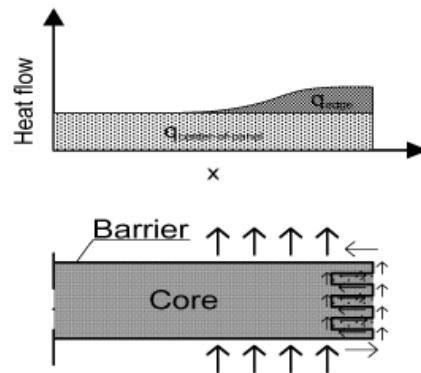


FIG. 2: With a serpentine edge the path for heat is prolonged with a smaller heat flow through the edge as the result.

Barrier type	Ψ_{edge} W/(m · K)
Serpentine 5 slots, depth 30 mm ¹ thickness of steel 0.1 mm	0.015
Serpentine > 15 slots, depth 30 mm ¹	<0.010

From the Licentiate Thesis of T.Torsell,

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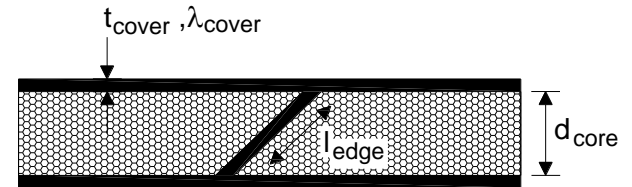
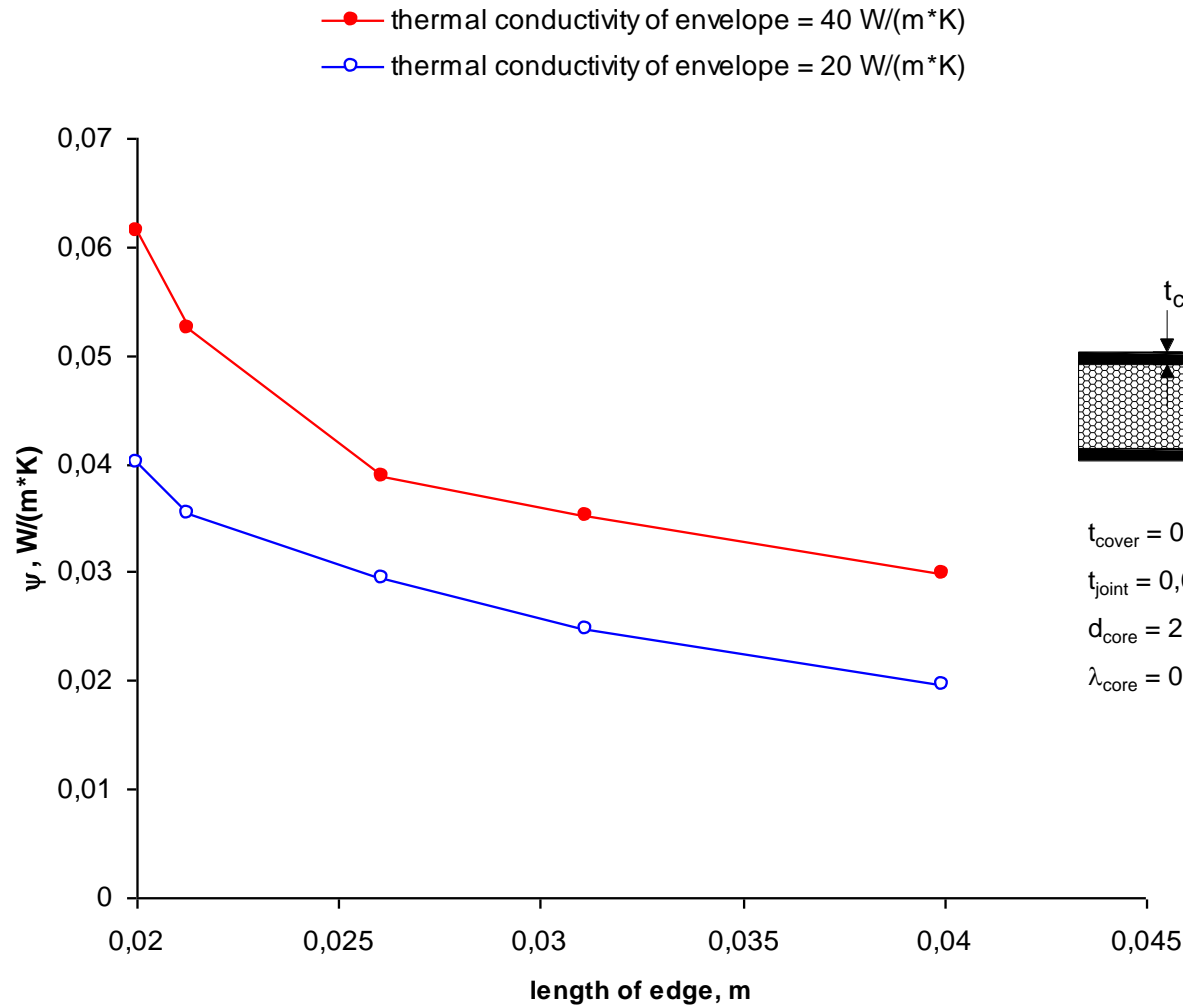
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edge length



$t_{\text{cover}} = 0,05 \text{ mm}$

$t_{\text{joint}} = 0,05 \text{ mm}$

$d_{\text{core}} = 20 \text{ mm}$

$\lambda_{\text{core}} = 0,004 \text{ W/(m·K)}$

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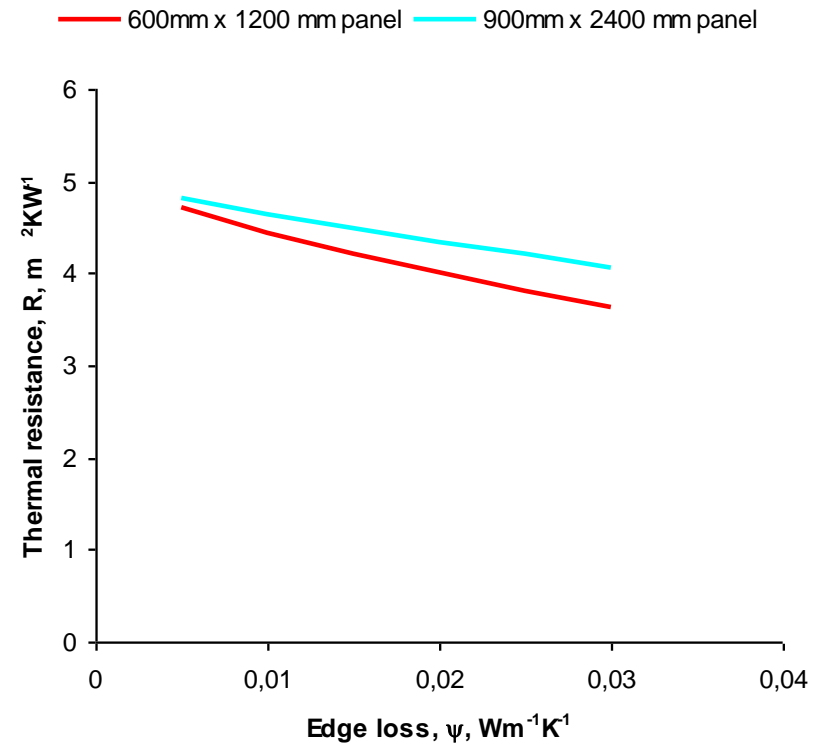
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Panel size



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Reduce thermal loss

Low thermal conductivity of envelope, especially joint

Adjacent insulation beneficiary

Thickness of cover secondary

Longer edge, substantial reduction

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All metal envelope of low conductivity metal such as stainless steel may provide a durable envelope.

The cover of that envelope can be made more robust with little effect on the heat loss at the edges.

Longer edges reduce edge loss

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